

PROCEEDINGS OF THE NEACRP SPECIALISTS' MEETING ON SHIELDING BENCHMARK CALCULATIONS

PARIS, JULY 1-2 1982

PART. I

LMFBR SHIELDING BENCHMARK

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LMFBR SHIELDING BENCHMARK

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Abstract

The present document summarizes the results and discussions relating to the LMFBR shielding benchmark exercise proposed by NEACRP in the report which is given in Annex I and which indicates the specifications of the LMFBR shielding benchmark. The PWR shielding benchmark also discussed at the meeting, will be the subject of a separate document.

Six different organisations participated in the LMFBR benchmark exercise, and eight solutions were submitted. The list of participants and contributors is given in Annex II.

General Comments

At the NEACRP Specialists' Meeting on "Neutron Data and Benchmarks for Reactor Shielding", held in Paris in October 1980, a formal programme of work was agreed upon for the execution of shielding benchmark studies.

It was considered that the status of multigroup cross section sets used by different laboratories had changed significantly in recent years and that it would be of interest for an international intercomparison to take advantage of the recent improvements in calculational techniques and the developments of sensitivity and uncertainty methods.

Actually, the major achievements of the previous meetings of this series had been in stimulating the development of data sensitivity analysis tools and stressing the need for appropriate data uncertainty information, both for meaningful design parameter uncertainty analysis and for effective use of benchmark single-material propagation experiments.

For the present meeting, it was agreed to limit the scope to an inter-comparison of the benchmark exercises. In the case of the LMFBR benchmark, the following quantities of interest were requested in the simplified 1D geometry:

- total, thermal equivalent and fast flux responses.
- steel damage dose
- activation rates of Na and Au
- fission rate of U-235
- neutron and γ -heating

All these values were requested at several positions, in the proposed geometrical model, representative in particular of the end of the lateral shield and of the wall of the secondary heat exchanger. The results obtained by the participants are given in Part I of the present document.

Part II of the document gives the details of the analysis of the results, in particular using the sensitivity coefficients provided by the participants.

The main results and conclusions of the exercise can be summarised as follows:

- The spread of the calculated results are much reduced with respect to the results obtained in a similar exercise, and compared at the Specialists' Meeting in Vienna in 1976.
- The observed discrepancies are often related to calculations performed by different laboratories using the same data base with different strategies to produce multigroup data (elastic and inelastic matrix production, composition dependent resonance self-shielding, etc.). This means that, in this area, the methods play a relevant rôle, which is still to be clarified. Continuous Monte Carlo calculations can certainly give useful information. However,

since in particular resonance self-shielding algorithms are, in general, well established, the problem of data processing could be handled more satisfactorily in the future with a more appropriate use of existing algorithms.

- The sensitivity coefficients provided by the participants were in excellent agreement, even when different perturbation codes were used. Thus, the present 1D techniques can be used with confidence for experiment analysis or design studies.
- The method approximation effects (angular quadrature, Legendre Polynomial order, mesh size) are well understood in 1D deep penetration calculations. Here again, an excellent agreement was found among the participants.
- Concerning the uncertainty analysis, it was clear from the data provided and from the discussions held at the meeting that data uncertainties and their correlations are still, to a large extent, lacking. The old Schmidt data are still being used together with the preliminary compilation performed at ORNL by Drischler and Weisbin.

It seems that in this field the data needs of the shielding community should be stressed in defining priorities in new data file versions (ENDF/B) or in the setting up of new evaluated data files, as it is the case for the Joint Evaluated File (JEF). In particular, data formats and data uncertainty types should fit the needs of transport calculations. The type of uncertainties and of correlations needed for sensitivity analysis as indicated by McCracken at Vienna in 1976 could represent a useful guideline. Moreover, shielding-oriented test problems should be included in the usual physical file checking phases.

The relation of the theoretical benchmark to experimental benchmarks was only partially discussed. In this respect, possible motivations for future specialists' meetings have also been discussed. It was generally agreed that the use of the experimental benchmark to improve shielding design calculations is still a field of high interest. However, the following points should be considered to define appropriate strategies to benefit from the experimental benchmarks:

- According to the conclusions of the present meeting, standard data processing procedures should be defined and their related uncertainty stated.
- Data uncertainty variance-covariance matrix information should be made available in appropriate formats for the major isotopes of interest for shielding (O-16 , Na , SS isotopes, etc.) in the principle evaluated data files.
- The present experimental benchmarks (in Fe) should be made available in standard format, including experimental results reduced to 1D models (i.e. with calculated corrections from the actual geometry to 1D model, to be specified), and this to allow a more generalised use of them. Moreover, the new planned experimental benchmark results (propagation in Na, EURACOS), should be made available within a reasonable time delay (mid-1983).

- Data adjustment and consistency procedures should be compared and analysed to define their applicability to shielding design needs.

The above mentioned topics seem to represent the fields in which most progress should be made in the near future, and their discussion, in a reasonable delay of time (about two years), should allow effective progress towards a substantial improvement of the present methods and data used in shielding design calculations and predictions.

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PART I
BENCHMARK RESULTS

The data origin of eight data sets used by the participants is the following:

- VITAMIN-E : ORNL generated 174 group cross-section data based on ENDF/B-V.
- VITAMIN-C : ORNL generated 171 group cross-section data based on ENDF/B-IV.
- RADHEAT : 100n - 20 gamma group library, based on ENDF/B-IV (neutrons), and POPOP-4 library ($n \rightarrow \gamma$), processed by the RADHEAT-V3 code system of JAERI.
- BABEL : 113n - 36 gamma group library, based on ENDF/B-IV, processed by the MCC2-PN code system, generated at CEA.
- PROPANE-D₀ : Shielding formulaire developed with the collaboration of CEA (France) and ENEA (Italy), based on 45 energy group data for neutrons and derived from BABEL.
- PROPANE-D₁ : Adjusted version of the previous formulaire, using neutron propagation experiments performed jointly by CEA and ENEA.
- EURLIB : EURLIB-3, as used by the UK.
- UKAEA : UKNDL processed in 100-group EURLIB structure Fe weighted with $\phi = [E\Sigma(E)]^{-1}$ and other isotopes with $\phi = E^{-1}$.

The following tables are provided:

- TABLES 1-3 : Major response function values as required.
- TABLES 4-8 : Sensitivity coefficients in the 15 energy group structure by isotope : Fe, Cr, Ni, Na in lateral shield, Na in Sodium tank. These are region integrated sensitivity coefficients S_a , S_s and S_t for $\Sigma_{\text{absorption}}$, $\Sigma_{\text{scattering}}$ (elastic + inelastic), and for the sum of the two Σ 's. The elastic contribution includes only the P_0 component. The sensitivity coefficients are for the following responses:
- ϕ_{tot} at mesh 62 and 187.
- ϕ 100 KeV at mesh 62.
- TABLE 9 : Sensitivity of ϕ_{tot} at mesh 62 to angular source values.
- TABLES 10-19 : 15 group cross-section values (Σ_a and Σ_s) supplied by the different participants.
- TABLES 20-44 : Results of the folding cross-section differences obtained from Tables 10-19 with the sensitivity coefficients S_a , S_s and S_t of Tables 4-8. There is one table for each isotope (Fe, Cr, Ni, Na) and one table of summary, and one set of tables for the following cases: (VITAMIN-E)-(BABEL), (RADHEAT)-(BABEL), (VITAMIN-C)-(BABEL), (PROPANE-D₁)-(PROPANE-D₀) and (VITAMIN-C). 910000016

| DATA SET | TOTAL FLUX | | | | NA-23 (N, GAMMA) | | | |
|----------|------------|-----------|-----------|-----------|------------------|-----------|-----------|-----------|
| | MESH 20 | MESH 62 | MESH 124 | MESH 187 | MESH 20 | MESH 62 | MESH 124 | MESH 187 |
| VITAM.-C | 3.430E+12 | 6.079E+08 | 3.836E+06 | 3.795E+03 | 5.759E+10 | 1.766E+07 | 4.534E+05 | 7.938E+02 |
| VITAM.-E | 3.584E+12 | 6.736E+08 | 4.063E+06 | 3.641E+03 | 4.522E+10 | 1.584E+07 | 4.276E+05 | 5.884E+02 |
| PADHEAT | 3.497E+12 | 6.001E+08 | 3.606E+06 | 3.303E+03 | 4.504E+10 | 1.430E+07 | 3.737E+05 | 5.208E+02 |
| BABEL | 3.200E+12 | 4.270E+08 | 2.440E+06 | 2.100E+03 | 4.400E+10 | 1.040E+07 | 2.320E+05 | 2.910E+02 |
| PROP.-D0 | 3.250E+12 | 4.370E+08 | 2.620E+06 | 2.580E+03 | 4.400E+10 | 1.060E+07 | 2.350E+05 | 3.400E+02 |
| PROP.-D1 | 3.590E+12 | 6.230E+08 | 4.310E+06 | 5.350E+03 | 4.810E+10 | 1.470E+07 | 3.740E+05 | 6.730E+02 |
| EURLIB | 3.710E+12 | 1.090E+09 | 8.300E+06 | 1.160E+04 | 4.870E+10 | 3.050E+07 | 1.540E+06 | 3.620E+03 |
| UKAEA | 4.060E+12 | 1.110E+09 | 1.280E+06 | 7.940E+03 | 5.470E+10 | 2.760E+07 | 8.070E+05 | 1.330E+03 |
| MEAN | 3.541E+12 | 6.961E+08 | 3.807E+06 | 5.039E+03 | 4.842E+10 | 1.770E+07 | 5.553E+05 | 1.020E+03 |
| ST. DEV. | 2.704E+11 | 2.643E+08 | 2.077E+06 | 3.224E+03 | 5.133E+09 | 7.460E+06 | 4.363E+05 | 1.099E+03 |

TABLE 1

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| | FLUX > 100 KEV | | | | DPA | | | |
|----------|----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| DATA SET | MESH 20 | MESH 62 | MESH 124 | MESH 187 | MESH 20 | MESH 62 | MESH 124 | MESH 187 |
| VITAM.-C | 3.301E+11 | 1.070E+07 | 4.644E+01 | 1.036E-03 | 1.256E+14 | 7.957E+09 | 9.169E+06 | 1.445E+04 |
| VITAM.-E | 3.340E+11 | 1.117E+07 | 7.712E+01 | 3.625E-03 | 1.276E+14 | 8.524E+09 | 8.662E+06 | 1.185E+04 |
| RADHEAT | 3.050E+11 | 9.725E+06 | 2.241E+01 | 3.889E-05 | 1.479E+14 | 8.409E+09 | 7.829E+06 | 1.077E+04 |
| BABEL | 2.580E+11 | 5.400E+06 | 1.930E+01 | 3.910E-04 | 1.180E+14 | 5.700E+09 | 6.240E+06 | 7.420E+03 |
| PROP.-D0 | 2.760E+11 | 6.600E+06 | 1.640E+01 | 1.400E-04 | 1.250E+14 | 5.950E+09 | 6.420E+06 | 8.710E+03 |
| PROP.-D1 | 3.010E+11 | 8.700E+06 | 2.600E+01 | 2.350E-04 | 1.370E+14 | 8.190E+09 | 1.040E+07 | 1.730E+04 |
| EURLIB | 4.280E+11 | 2.920E+07 | 4.970E+01 | 4.480E-05 | 1.420E+14 | 1.650E+10 | 3.190E+07 | 7.450E+04 |
| UKAEA | 4.030E+11 | 1.920E+07 | 2.280E+01 | 2.150E-05 | 1.370E+14 | 1.290E+10 | 1.670E+07 | 2.740E+04 |
| MEAN | 3.294E+11 | 1.259E+07 | 3.502E+01 | 6.915E-04 | 1.325E+14 | 9.266E+09 | 1.216E+07 | 2.155E+04 |
| ST. DEV. | 5.918E+10 | 7.893E+06 | 2.105E+01 | 1.232E-03 | 1.004E+13 | 3.653E+09 | 8.630E+06 | 2.230E+04 |

TABLE 2

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| DATA SET | THERMAL EQUIVALENT FLUX | | | | CO-59(N,GAMMA) | | | |
|----------|-------------------------|-----------|-----------|-----------|----------------|-----------|-----------|-----------|
| | MESH 20 | MESH 62 | MESH 124 | MESH 187 | MESH 20 | MESH 62 | MESH 124 | MESH 187 |
| VITAM.-C | 7.300E+10 | 2.995E+07 | 1.031E+06 | 1.690E+03 | 2.162E+13 | 4.807E+09 | 3.421E+07 | 4.283E+04 |
| VITAM.-E | 7.482E+10 | 3.103E+07 | 9.608E+05 | 1.364E+03 | 2.201E+13 | 5.213E+09 | 3.721E+07 | 4.241E+04 |
| RADHEAT | 4.585E+09 | 6.481E+06 | 4.475E+05 | 7.156E+02 | 2.078E+13 | 4.589E+09 | 3.322E+07 | 3.734E+04 |
| BABEL | 6.200E+10 | 1.630E+07 | 3.870E+05 | 4.780E+02 | 1.990E+13 | 3.410E+09 | 2.260E+07 | 2.350E+04 |
| PROP.-D0 | 6.200E+10 | 1.700E+07 | 3.920E+05 | 5.600E+02 | 2.020E+13 | 3.470E+09 | 2.390E+07 | 2.760E+04 |
| PROP.-D1 | 6.720E+10 | 2.350E+07 | 6.260E+05 | 1.110E+03 | 2.200E+13 | 4.950E+09 | 4.060E+07 | 5.490E+04 |
| EURLIB | 7.420E+10 | 5.250E+07 | 2.770E+06 | 6.470E+03 | 2.180E+13 | 8.500E+09 | 1.230E+08 | 2.570E+05 |
| UKAEA | 7.630E+10 | 4.520E+07 | 1.460E+06 | 2.410E+03 | 2.430E+13 | 8.620E+09 | 7.210E+07 | 9.550E+04 |
| MEAN | 6.176E+10 | 2.774E+07 | 1.009E+06 | 1.850E+03 | 2.158E+13 | 5.445E+09 | 4.835E+07 | 7.264E+04 |
| ST. DEV. | 2.379E+10 | 1.535E+07 | 8.051E+05 | 1.975E+03 | 1.372E+12 | 2.032E+09 | 3.383E+07 | 7.775E+04 |

TABLE 2 bis

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| | U-235(N,F) | | | | χ -HEATING | | μ -HEATING | |
|----------|------------|-----------|-----------|-----------|-----------------|-----------|----------------|-----------|
| DATA SET | MESH 20 | MESH 62 | MESH 124 | MESH 187 | MESH 20 | MESH 62 | MESH 20 | MESH 62 |
| VITAM.-C | 6.252E+13 | 1.762E+10 | 3.682E+08 | 5.551E+05 | 1.545E-02 | 4.585E-06 | 2.374E-04 | 2.921E-03 |
| VITAM.-C | 6.566E+13 | 1.981E+10 | 4.072E+08 | 5.464E+05 | 1.568E-02 | 4.988E-06 | 2.443E-04 | 3.229E-03 |
| RADHEAT | 6.962E+13 | 1.952E+10 | 3.830E+08 | 5.006E+05 | 1.354E-02 | 3.981E-06 | 1.731E-04 | 9.596E-03 |
| BABEL | 5.440E+13 | 1.220E+10 | 2.430E+08 | 3.010E+05 | 1.600E-02 | 3.930E-06 | 2.270E-04 | 2.650E-03 |
| PROP.-D0 | 5.460E+13 | 1.230E+10 | 2.460E+08 | 3.510E+05 | 1.640E-02 | 4.000E-06 | 2.370E-04 | 2.720E-03 |
| PROP.-D1 | 5.960E+13 | 1.730E+10 | 3.940E+08 | 6.190E+05 | 1.750E-02 | 4.790E-06 | 2.600E-04 | 3.810E-03 |
| EURLIB | 6.780E+13 | 3.760E+10 | 1.620E+09 | 3.820E+06 | 0.0 | 0.0 | 0.0 | 0.0 |
| UKAEA | 7.210E+13 | 3.330E+10 | 8.010E+08 | 1.270E+06 | 0.0 | 0.0 | 0.0 | 0.0 |
| MEAN | 6.329E+13 | 2.121E+10 | 5.578E+08 | 9.954E+05 | 1.576E-02 | 4.379E-06 | 2.298E-04 | 2.715E-03 |
| ST. DEV. | 6.681E+12 | 9.323E+09 | 4.629E+08 | 1.179E+06 | 1.306E-03 | 4.661E-07 | 2.985E-05 | 9.583E-03 |

TABLE 3

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| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -2.881E-03 | -1.161E-01 | -1.189E-01 | -9.091E-04 | -3.003E-02 | -3.094E-02 | -9.634E-04 | -3.223E-02 | -3.320E-02 |
| 2 | -2.636E-03 | -3.636E-01 | -3.663E-01 | -8.370E-04 | -9.267E-02 | -9.350E-02 | -8.867E-04 | -9.958E-02 | -1.005E-01 |
| 3 | -2.562E-03 | -1.043E+00 | -1.045E+00 | -7.218E-04 | -2.116E-01 | -2.123E-01 | -7.695E-04 | -2.308E-01 | -2.315E-01 |
| 4 | -1.344E-02 | -2.419E+00 | -2.432E+00 | -3.491E-03 | -4.558E-01 | -4.593E-01 | -3.733E-03 | -4.988E-01 | -5.025E-01 |
| 5 | -1.015E-02 | -1.169E+00 | -1.179E+00 | -3.506E-03 | -2.596E-01 | -2.631E-01 | -3.705E-03 | -2.821E-01 | -2.856E-01 |
| 6 | -1.363E-02 | -1.839E+00 | -1.853E+00 | -5.725E-03 | -4.500E-01 | -4.557E-01 | -6.002E-03 | -4.875E-01 | -4.935E-01 |
| 7 | -1.569E-02 | -1.803E+00 | -1.819E+00 | -8.087E-03 | -4.771E-01 | -4.851E-01 | -8.445E-03 | -5.159E-01 | -5.243E-01 |
| 8 | -8.328E-04 | -2.271E-01 | -2.280E-01 | -2.197E-03 | -1.571E-01 | -1.593E-01 | -2.238E-03 | -1.656E-01 | -1.678E-01 |
| 9 | 0.0 | 0.0 | 0.0 | -7.542E-02 | -2.044E+00 | -2.120E+00 | -7.886E-02 | -2.224E+00 | -2.303E+00 |
| 10 | 0.0 | 0.0 | 0.0 | -1.927E-02 | -5.062E-01 | -5.255E-01 | -1.744E-02 | -4.919E-01 | -5.094E-01 |
| 11 | 0.0 | 0.0 | 0.0 | -1.678E-02 | -2.203E-01 | -2.371E-01 | -1.459E-02 | -2.039E-01 | -2.185E-01 |
| 12 | 0.0 | 0.0 | 0.0 | -2.734E-02 | -1.875E-01 | -2.149E-01 | -2.243E-02 | -1.533E-01 | -1.758E-01 |
| 13 | 0.0 | 0.0 | 0.0 | -1.787E-01 | -4.301E-01 | -6.088E-01 | -1.492E-01 | -4.360E-01 | -5.852E-01 |
| 14 | 0.0 | 0.0 | 0.0 | -1.704E-01 | -4.919E-01 | -6.624E-01 | -1.182E-01 | -3.404E-01 | -4.586E-01 |
| 15 | 0.0 | 0.0 | 0.0 | -1.009E-01 | -4.865E-02 | -1.496E-01 | -1.251E-01 | 8.510E-02 | -4.002E-02 |
| SUM | -6.183E-02 | -8.979E+00 | -9.041E+00 | -6.143E-01 | -6.063E+00 | -6.677E+00 | -5.526E-01 | -6.077E+00 | -6.630E+00 |

TABLE 4 - SENSITIVITY COEFFICIENTS FE

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| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -2.643E-04 | -2.873E-02 | -2.899E-02 | -8.340E-05 | -7.480E-03 | -7.563E-03 | -8.837E-05 | -8.023E-03 | -8.111E-03 |
| 2 | -2.842E-04 | -1.060E-01 | -1.063E-01 | -9.023E-05 | -2.688E-02 | -2.697E-02 | -9.559E-05 | -2.889E-02 | -2.899E-02 |
| 3 | -1.429E-03 | -3.174E-01 | -3.188E-01 | -4.025E-04 | -6.819E-02 | -6.859E-02 | -4.291E-04 | -7.412E-02 | -7.454E-02 |
| 4 | -6.572E-03 | -5.245E-01 | -5.311E-01 | -1.707E-03 | -9.808E-02 | -9.978E-02 | -1.825E-03 | -1.073E-01 | -1.091E-01 |
| 5 | -2.234E-03 | -5.069E-01 | -5.091E-01 | -7.715E-04 | -1.117E-01 | -1.124E-01 | -8.152E-04 | -1.215E-01 | -1.223E-01 |
| 6 | -2.768E-03 | -5.402E-01 | -5.430E-01 | -1.163E-03 | -1.321E-01 | -1.332E-01 | -1.219E-03 | -1.431E-01 | -1.443E-01 |
| 7 | -3.385E-03 | -5.848E-01 | -5.882E-01 | -1.745E-03 | -1.508E-01 | -1.525E-01 | -1.822E-03 | -1.633E-01 | -1.651E-01 |
| 8 | -9.670E-05 | -4.817E-02 | -4.827E-02 | -2.552E-04 | -3.384E-02 | -3.410E-02 | -2.598E-04 | -3.565E-02 | -3.591E-02 |
| 9 | 0.0 | 0.0 | 0.0 | -2.038E-02 | -8.165E-01 | -8.369E-01 | -2.131E-02 | -8.888E-01 | -9.101E-01 |
| 10 | 0.0 | 0.0 | 0.0 | -1.007E-02 | -6.134E-02 | -7.141E-02 | -9.114E-03 | -5.896E-02 | -6.807E-02 |
| 11 | 0.0 | 0.0 | 0.0 | -1.888E-02 | -5.745E-02 | -7.633E-02 | -1.641E-02 | -5.344E-02 | -6.985E-02 |
| 12 | 0.0 | 0.0 | 0.0 | -5.712E-02 | -7.133E-02 | -1.285E-01 | -4.687E-02 | -5.888E-02 | -1.057E-01 |
| 13 | 0.0 | 0.0 | 0.0 | -1.701E-02 | -5.302E-02 | -7.003E-02 | -1.420E-02 | -5.339E-02 | -6.759E-02 |
| 14 | 0.0 | 0.0 | 0.0 | -5.605E-02 | -5.195E-02 | -1.080E-01 | -3.886E-02 | -3.615E-02 | -7.501E-02 |
| 15 | 0.0 | 0.0 | 0.0 | -3.224E-02 | -4.959E-03 | -3.720E-02 | -3.991E-02 | 8.702E-03 | -3.121E-02 |
| SUM | -1.703E-02 | -2.657E+00 | -2.674E+00 | -2.180E-01 | -1.746E+00 | -1.964E+00 | -1.932E-01 | -1.823E+00 | -2.016E+00 |

TABLE 5 - SENSITIVITY COEFFICIENTS CR

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -3.726E-03 | -1.320E-02 | -1.692E-02 | -1.176E-03 | -3.468E-03 | -4.643E-03 | -1.246E-03 | -3.719E-03 | -4.965E-03 |
| 2 | -5.305E-03 | -4.830E-02 | -5.360E-02 | -1.685E-03 | -1.220E-02 | -1.388E-02 | -1.785E-03 | -1.312E-02 | -1.491E-02 |
| 3 | -3.936E-03 | -1.368E-01 | -1.408E-01 | -1.109E-03 | -2.971E-02 | -3.081E-02 | -1.182E-03 | -3.226E-02 | -3.344E-02 |
| 4 | -3.909E-03 | -2.496E-01 | -2.535E-01 | -1.015E-03 | -4.531E-02 | -4.632E-02 | -1.085E-03 | -4.963E-02 | -5.072E-02 |
| 5 | -1.981E-03 | -2.117E-01 | -2.137E-01 | -6.841E-04 | -4.745E-02 | -4.814E-02 | -7.228E-04 | -5.154E-02 | -5.226E-02 |
| 6 | -2.858E-03 | -2.168E-01 | -2.197E-01 | -1.200E-03 | -5.455E-02 | -5.575E-02 | -1.258E-03 | -5.896E-02 | -6.021E-02 |
| 7 | -3.352E-03 | -5.315E-01 | -5.348E-01 | -1.727E-03 | -1.362E-01 | -1.379E-01 | -1.804E-03 | -1.475E-01 | -1.493E-01 |
| 8 | -1.822E-04 | -6.743E-02 | -6.761E-02 | -4.807E-04 | -4.683E-02 | -4.731E-02 | -4.896E-04 | -4.934E-02 | -4.983E-02 |
| 9 | 0.0 | 0.0 | 0.0 | -2.105E-02 | -7.866E-01 | -8.077E-01 | -2.201E-02 | -8.600E-01 | -8.820E-01 |
| 10 | 0.0 | 0.0 | 0.0 | -7.763E-03 | -7.664E-02 | -8.440E-02 | -7.027E-03 | -7.409E-02 | -8.111E-02 |
| 11 | 0.0 | 0.0 | 0.0 | -1.302E-02 | -4.289E-01 | -4.419E-01 | -1.132E-02 | -4.035E-01 | -4.148E-01 |
| 12 | 0.0 | 0.0 | 0.0 | -1.600E-02 | -6.434E-02 | -8.034E-02 | -1.313E-02 | -5.294E-02 | -6.607E-02 |
| 13 | 0.0 | 0.0 | 0.0 | -1.124E-02 | -9.189E-02 | -1.031E-01 | -9.389E-03 | -9.252E-02 | -1.019E-01 |
| 14 | 0.0 | 0.0 | 0.0 | -4.034E-02 | -9.946E-02 | -1.398E-01 | -2.798E-02 | -6.854E-02 | -9.652E-02 |
| 15 | 0.0 | 0.0 | 0.0 | -2.352E-02 | -1.004E-02 | -3.355E-02 | -2.921E-02 | 1.770E-02 | -1.151E-02 |
| SUM | -2.525E-02 | -1.475E+00 | -1.501E+00 | -1.420E-01 | -1.934E+00 | -2.076E+00 | -1.296E-01 | -1.940E+00 | -2.070E+00 |

TABLE 6 - SENSITIVITY COEFFICIENTS NI

91080016

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -5.547E-04 | -1.755E-02 | -1.810E-02 | -1.750E-04 | -4.537E-03 | -4.712E-03 | -1.855E-04 | -4.869E-03 | -5.054E-03 |
| 2 | -1.904E-05 | -8.034E-02 | -8.036E-02 | -6.045E-06 | -2.054E-02 | -2.054E-02 | -6.404E-06 | -2.206E-02 | -2.207E-02 |
| 3 | -6.910E-05 | -2.777E-01 | -2.777E-01 | -1.947E-05 | -5.754E-02 | -5.756E-02 | -2.075E-05 | -6.262E-02 | -6.264E-02 |
| 4 | -2.998E-04 | -1.624E+00 | -1.624E+00 | -7.785E-05 | -2.714E-01 | -2.714E-01 | -8.323E-05 | -2.997E-01 | -2.998E-01 |
| 5 | -2.224E-04 | -1.147E+00 | -1.147E+00 | -7.681E-05 | -2.488E-01 | -2.489E-01 | -8.116E-05 | -2.713E-01 | -2.714E-01 |
| 6 | -2.414E-04 | -7.498E-01 | -7.500E-01 | -1.014E-04 | -1.777E-01 | -1.778E-01 | -1.063E-04 | -1.931E-01 | -1.932E-01 |
| 7 | -4.834E-04 | -1.471E+00 | -1.471E+00 | -2.492E-04 | -3.724E-01 | -3.727E-01 | -2.602E-04 | -4.038E-01 | -4.041E-01 |
| 8 | -3.544E-05 | -1.142E-01 | -1.142E-01 | -9.353E-05 | -7.197E-02 | -7.206E-02 | -9.524E-05 | -7.594E-02 | -7.604E-02 |
| 9 | 0.0 | 0.0 | 0.0 | -3.311E-03 | -1.247E+00 | -1.250E+00 | -3.462E-03 | -1.364E+00 | -1.368E+00 |
| 10 | 0.0 | 0.0 | 0.0 | -1.678E-03 | -1.327E-01 | -1.344E-01 | -1.519E-03 | -1.290E-01 | -1.305E-01 |
| 11 | 0.0 | 0.0 | 0.0 | -1.549E-04 | -1.329E-01 | -1.331E-01 | -1.347E-04 | -1.246E-01 | -1.247E-01 |
| 12 | 0.0 | 0.0 | 0.0 | -6.140E-03 | -1.204E-01 | -1.286E-01 | -6.678E-03 | -9.845E-02 | -1.051E-01 |
| 13 | 0.0 | 0.0 | 0.0 | -7.713E-03 | -6.763E-02 | -7.534E-02 | -6.491E-03 | -7.070E-02 | -7.719E-02 |
| 14 | 0.0 | 0.0 | 0.0 | -1.240E-02 | -6.704E-02 | -7.944E-02 | -1.253E-02 | -4.391E-02 | -5.644E-02 |
| 15 | 0.0 | 0.0 | 0.0 | -6.873E-03 | -4.390E-03 | -1.126E-02 | -4.776E-02 | 5.376E-02 | 6.003E-03 |
| SUM | -1.925E-03 | -5.481E+00 | -5.483E+00 | -4.107E-02 | -2.997E+00 | -3.038E+00 | -7.941E-02 | -3.111E+00 | -3.190E+00 |

TABLE 7 - SENSITIVITY COEFFICIENTS NA IN LATERAL SHIELD

91080016

| GROUP | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -2.482E-08 | 3.756E-07 | 3.508E-07 | -1.981E-10 | 1.607E-09 | 1.409E-09 | -2.933E-09 | -2.986E-08 | -3.280E-08 |
| 2 | -1.116E-09 | 4.908E-06 | 4.907E-06 | -9.015E-12 | 1.859E-08 | 1.858E-08 | -8.018E-11 | -2.615E-07 | -2.615E-07 |
| 3 | -8.178E-08 | 3.387E-04 | 3.386E-04 | -6.805E-10 | 1.237E-06 | 1.236E-06 | -4.303E-09 | -1.246E-05 | -1.247E-05 |
| 4 | -3.085E-06 | 6.292E-03 | 6.289E-03 | -2.418E-05 | 2.226E-05 | 2.224E-05 | -7.578E-08 | -1.271E-04 | -1.272E-04 |
| 5 | -5.629E-06 | 5.631E-03 | 5.626E-03 | -4.619E-08 | 2.482E-05 | 2.477E-05 | -1.358E-07 | -1.385E-04 | -1.386E-04 |
| 6 | -2.240E-05 | 1.981E-02 | 1.979E-02 | -2.344E-07 | 1.695E-04 | 1.693E-04 | -9.113E-07 | -1.286E-03 | -1.287E-03 |
| 7 | -8.733E-05 | 1.052E-02 | 1.043E-02 | -1.475E-06 | 6.047E-04 | 6.033E-04 | -4.770E-06 | -3.514E-03 | -3.519E-03 |
| 8 | -3.844E-05 | -8.203E-02 | -8.206E-02 | -1.491E-06 | 4.422E-04 | 4.407E-04 | -5.281E-06 | -2.892E-03 | -2.897E-03 |
| 9 | 0.0 | 0.0 | 0.0 | -1.584E-04 | 2.350E-02 | 2.334E-02 | -5.269E-04 | -1.567E-01 | -1.572E-01 |
| 10 | 0.0 | 0.0 | 0.0 | -5.468E-04 | 1.385E-02 | 1.330E-02 | -1.796E-03 | -1.174E-01 | -1.192E-01 |
| 11 | 0.0 | 0.0 | 0.0 | -6.225E-05 | 2.339E-02 | 2.332E-02 | -1.997E-04 | -1.589E-01 | -1.591E-01 |
| 12 | 0.0 | 0.0 | 0.0 | -3.447E-03 | -5.932E-04 | -4.040E-03 | -9.831E-03 | -8.991E-02 | -9.974E-02 |
| 13 | 0.0 | 0.0 | 0.0 | -9.323E-03 | 4.068E-02 | 3.136E-02 | -6.668E-02 | -1.268E+00 | -1.334E+00 |
| 14 | 0.0 | 0.0 | 0.0 | -2.588E-02 | 4.277E-02 | 1.689E-02 | -3.790E-01 | -3.953E+00 | -4.332E+00 |
| 15 | 0.0 | 0.0 | 0.0 | -9.020E-02 | 3.537E-02 | -5.483E-02 | -2.182E+00 | -1.766E+00 | -3.948E+00 |
| SUM | -1.570E-04 | -3.942E-02 | -3.950E-02 | -1.296E-01 | 1.802E-01 | 5.060E-02 | -2.640E+00 | -7.517E+00 | -1.016E+01 |

TABLE 8 - SENSITIVITY COEFFICIENTS NA IN NA TANK

SENSITIVITY TO ANGULAR SOURCE IN POINT 1

| GRP. | ANGLE | N = 1 | N = 2 | N = 3 | N = 4 | N = 5 |
|------|-------|-------|-------------|-------------|-------------|-------------|
| 1 | 0.0 | | 1.92608E-06 | 9.87623E-06 | 8.42146E-03 | 1.95398E-02 |
| 2 | 0.0 | | 9.68038E-06 | 3.44461E-05 | 2.67781E-02 | 6.10190E-02 |
| 3 | 0.0 | | 1.94790E-05 | 5.50621E-05 | 4.37362E-02 | 1.00602E-01 |
| 4 | 0.0 | | 3.37812E-05 | 9.37240E-05 | 6.71297E-02 | 1.51196E-01 |
| 5 | 0.0 | | 1.59807E-05 | 4.37996E-05 | 3.56493E-02 | 8.39731E-02 |
| 6 | 0.0 | | 1.83782E-05 | 4.51470E-05 | 2.85132E-02 | 6.35739E-02 |
| 7 | 0.0 | | 1.39681E-05 | 3.24735E-05 | 2.29151E-02 | 5.28771E-02 |
| 8 | 0.0 | | 2.94015E-06 | 7.07782E-06 | 5.17792E-03 | 1.23423E-02 |
| 9 | 0.0 | | 6.15669E-05 | 1.28221E-04 | 6.66926E-02 | 1.46856E-01 |
| 10 | 0.0 | | 1.38050E-06 | 2.75709E-06 | 1.04846E-03 | 2.31255E-03 |
| 11 | 0.0 | | 6.49548E-07 | 1.28600E-06 | 4.88885E-04 | 1.08747E-03 |
| 12 | 0.0 | | 3.79978E-07 | 7.36335E-07 | 1.44111E-04 | 3.04646E-04 |
| 13 | 0.0 | | 8.51765E-08 | 1.65973E-07 | 3.98189E-05 | 8.50652E-05 |
| 14 | 0.0 | | 3.25830E-09 | 6.33458E-09 | 1.40113E-06 | 2.98325E-06 |
| 15 | 0.0 | | 8.98734E-13 | 1.74242E-12 | 3.78065E-10 | 8.19169E-10 |

TABLE 9 - SENSITIVITY TO THE SOURCE

91080016

| DATA SET | GROUP 1 | GROUP 2 | GROUP 3 | GROUP 4 | GROUP 5 | GROUP 6 | GROUP 7 | GROUP 8 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 4.327E-02 | 1.041E-02 | 2.533E-03 | 3.699E-03 | 5.156E-03 | 4.971E-03 | 5.047E-03 | 5.329E-03 |
| VITAM.-F | 4.344E-02 | 1.057E-02 | 2.632E-03 | 4.840E-03 | 6.339E-03 | 4.684E-03 | 3.685E-03 | 4.159E-03 |
| RADHEAT | 4.716E-04 | 8.598E-04 | 1.590E-03 | 3.861E-03 | 5.142E-03 | 4.952E-03 | 5.047E-03 | 5.328E-03 |
| BABEL | 4.251E-02 | 9.581E-03 | 2.404E-03 | 3.861E-03 | 5.144E-03 | 4.948E-03 | 5.041E-03 | 5.324E-03 |
| PROP.-DC | 3.401E-02 | 6.269E-03 | 2.153E-03 | 3.865E-03 | 5.142E-03 | 4.946E-03 | 5.045E-03 | 5.323E-03 |
| PROP.-D1 | 3.374E-02 | 6.255E-03 | 2.149E-03 | 3.857E-03 | 5.126E-03 | 4.922E-03 | 5.012E-03 | 5.258E-03 |
| EURLIB | 4.327E-02 | 9.614E-03 | 2.396E-03 | 3.881E-03 | 5.145E-03 | 4.950E-03 | 5.048E-03 | 5.349E-03 |
| UKAEA | 4.244E-02 | 8.201E-03 | 2.409E-03 | 4.058E-03 | 5.242E-03 | 4.983E-03 | 4.474E-03 | 3.574E-03 |
| MEAN | 3.539E-02 | 7.720E-03 | 2.283E-03 | 3.990E-03 | 5.305E-03 | 4.920E-03 | 4.800E-03 | 4.955E-03 |
| ST. DEV. | 1.470E-02 | 3.251E-03 | 3.256E-04 | 3.566E-04 | 4.195E-04 | 9.682E-05 | 4.924E-04 | 6.907E-04 |

TABLE 10 - Fe σ_a 10⁻⁶

| DATA SET | GROUP 9 | GROUP 10 | GROUP 11 | GROUP 12 | GROUP 13 | GROUP 14 | GROUP 15 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 7.027E-03 | 8.272E-03 | 7.711E-03 | 1.291E-02 | 5.205E-02 | 5.942E-02 | 2.487E-01 |
| VITAM.-E | 6.301E-03 | 7.617E-03 | 8.548E-03 | 1.035E-02 | 4.390E-02 | 5.713E-02 | 2.492E-01 |
| RADHEAT | 7.159E-03 | 5.625E-03 | 8.699E-03 | 1.225E-02 | 4.418E-02 | 5.912E-02 | 2.492E-01 |
| BABEL | 7.036E-03 | 9.628E-03 | 8.161E-03 | 1.308E-02 | 6.689E-02 | 5.917E-02 | 2.456E-01 |
| PROP.-D0 | 7.042E-03 | 1.054E-02 | 6.670E-03 | 1.247E-02 | 7.667E-02 | 6.325E-02 | 2.728E-01 |
| PROP.-D1 | 7.009E-03 | 1.044E-02 | 6.645E-03 | 1.210E-02 | 6.791E-02 | 6.296E-02 | 2.728E-01 |
| EURLIB | 7.047E-03 | 7.818E-03 | 6.410E-03 | 1.193E-02 | 4.634E-02 | 5.896E-02 | 2.334E-01 |
| UKAEA | 7.244E-03 | 7.045E-03 | 5.959E-03 | 9.173E-03 | 3.829E-02 | 5.686E-02 | 2.320E-01 |
| MEAN | 6.983E-03 | 8.373E-03 | 7.350E-03 | 1.178E-02 | 5.453E-02 | 5.961E-02 | 2.505E-01 |
| ST. DEV. | 2.872E-04 | 1.721E-03 | 1.057E-03 | 1.342E-03 | 1.404E-02 | 2.363E-03 | 1.539E-02 |

TABLE 10 (contd.) - Fe σ_a

600016

| DATA SET | GROUP 1 | GROUP 2 | GROUP 3 | GROUP 4 | GROUP 5 | GROUP 6 | GROUP 7 | GROUP 8 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 3.598E+00 | 3.394E+00 | 2.920E+00 | 2.725E+00 | 1.936E+00 | 3.262E+00 | 2.550E+00 | 2.798E+00 |
| VITAM.-E | 3.597E+00 | 3.394E+00 | 2.926E+00 | 2.735E+00 | 1.936E+00 | 3.270E+00 | 2.562E+00 | 2.615E+00 |
| RADHEAT | 3.642E+00 | 3.448E+00 | 2.879E+00 | 2.688E+00 | 2.033E+00 | 3.326E+00 | 2.575E+00 | 2.727E+00 |
| BABEL | 3.602E+00 | 3.457E+00 | 2.951E+00 | 2.878E+00 | 2.213E+00 | 3.537E+00 | 2.805E+00 | 2.894E+00 |
| PROP.-D0 | 3.594E+00 | 3.300E+00 | 2.912E+00 | 2.835E+00 | 2.225E+00 | 3.556E+00 | 2.788E+00 | 2.872E+00 |
| PROP.-D1 | 3.585E+00 | 3.285E+00 | 2.907E+00 | 2.829E+00 | 2.217E+00 | 3.543E+00 | 2.776E+00 | 2.864E+00 |
| EURLIB | 3.596E+00 | 3.423E+00 | 2.756E+00 | 2.387E+00 | 1.732E+00 | 2.994E+00 | 1.807E+00 | 2.077E+00 |
| UKAEA | 3.605E+00 | 3.469E+00 | 2.999E+00 | 2.611E+00 | 1.692E+00 | 2.998E+00 | 1.785E+00 | 2.462E+00 |
| MEAN | 3.602E+00 | 3.396E+00 | 2.906E+00 | 2.711E+00 | 2.004E+00 | 3.311E+00 | 2.456E+00 | 2.664E+00 |
| ST. DEV. | 1.790E-02 | 7.010E-02 | 7.033E-02 | 1.574E-01 | 2.051E-01 | 2.292E-01 | 4.210E-01 | 2.792E-01 |

TABLE 11 - Fe σ_s

910800
10

| DATA SET | GROUP 9 | GROUP 10 | GROUP 11 | GROUP 12 | GROUP 13 | GROUP 14 | GROUP 15 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 3.429E+00 | 5.623E+00 | 3.468E+00 | 7.053E+00 | 9.978E+00 | 1.138E+01 | 1.140E+01 |
| VITAM.-E | 3.339E+00 | 5.616E+00 | 3.504E+00 | 7.015E+00 | 9.890E+00 | 1.136E+01 | 1.141E+01 |
| RADHEAT | 3.463E+00 | 5.707E+00 | 5.860E+00 | 7.045E+00 | 9.974E+00 | 1.138E+01 | 1.140E+01 |
| BABEL | 3.471E+00 | 5.644E+00 | 3.655E+00 | 6.909E+00 | 9.975E+00 | 1.138E+01 | 1.140E+01 |
| PROP.-D0 | 3.450E+00 | 7.365E+00 | 1.271E+00 | 7.143E+00 | 1.013E+01 | 1.137E+01 | 1.140E+01 |
| PROP.-D1 | 3.448E+00 | 7.271E+00 | 1.249E+00 | 7.017E+00 | 1.007E+01 | 1.136E+01 | 1.140E+01 |
| EURLIB | 2.718E+00 | 5.779E+00 | 3.597E+00 | 6.791E+00 | 9.975E+00 | 1.137E+01 | 1.139E+01 |
| UKAEA | 2.598E+00 | 5.230E+00 | 3.722E+00 | 7.015E+00 | 9.474E+00 | 1.108E+01 | 1.134E+01 |
| MEAN | 3.239E+00 | 6.029E+00 | 3.291E+00 | 6.998E+00 | 9.933E+00 | 1.133E+01 | 1.139E+01 |
| ST. DEV. | 3.628E-01 | 8.120E-01 | 1.480E+00 | 1.056E-01 | 1.990E-01 | 1.021E-01 | 2.287E-02 |

TABLE 11 (contd.) - Fe σ_S

0100800000

| DATA SET | GROUP 1 | GROUP 2 | GROUP 3 | GROUP 4 | GROUP 5 | GROUP 6 | GROUP 7 | GROUP 8 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 1.663E-02 | 3.941E-03 | 4.907E-03 | 7.125E-03 | 4.464E-03 | 3.804E-03 | 3.781E-03 | 2.232E-03 |
| VITAM.-E | 3.945E-02 | 7.001E-03 | 5.085E-03 | 2.296E-02 | 9.904E-03 | 3.792E-03 | 3.772E-03 | 2.207E-03 |
| RADHEAT | 7.867E-04 | 2.423E-03 | 4.959E-03 | 7.017E-03 | 4.119E-03 | 3.721E-03 | 3.797E-03 | 2.276E-03 |
| BABEL | 1.451E-02 | 3.843E-03 | 4.987E-03 | 7.023E-03 | 4.212E-03 | 3.739E-03 | 4.047E-03 | 2.300E-03 |
| PROP.-D0 | 1.143E-02 | 3.535E-03 | 5.432E-03 | 7.005E-03 | 4.205E-03 | 3.737E-03 | 4.059E-03 | 2.283E-03 |
| PROP.-D1 | 1.135E-02 | 3.532E-03 | 5.420E-03 | 6.994E-03 | 4.194E-03 | 3.723E-03 | 4.033E-03 | 2.258E-03 |
| EURLIB | 1.660E-02 | 3.844E-03 | 4.991E-03 | 7.014E-03 | 4.209E-03 | 3.738E-03 | 4.026E-03 | 2.418E-03 |
| UKAEA | 7.377E-03 | 1.616E-03 | 2.088E-03 | 3.554E-03 | 3.366E-03 | 3.179E-03 | 4.811E-03 | 3.879E-03 |
| MEAN | 1.477E-02 | 3.717E-03 | 4.734E-03 | 8.587E-03 | 4.836E-03 | 3.679E-03 | 4.041E-03 | 2.482E-03 |
| ST. DEV. | 1.127E-02 | 1.559E-03 | 1.089E-03 | 5.934E-03 | 2.071E-03 | 2.043E-04 | 3.368E-04 | 5.682E-04 |

TABLE 12 - Cr σ_{α}

| DATA SET | GROUP 9 | GROUP 10 | GROUP 11 | GROUP 12 | GROUP 13 | GROUP 14 | GROUP 15 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 6.991E-03 | 1.867E-02 | 3.208E-02 | 8.934E-02 | 2.396E-02 | 7.254E-02 | 3.010E-01 |
| VITAM.-E | 6.867E-03 | 1.859E-02 | 3.207E-02 | 8.733E-02 | 2.387E-02 | 7.266E-02 | 3.029E-01 |
| RADHEAT | 6.896E-03 | 1.796E-02 | 3.108E-02 | 7.361E-02 | 2.378E-02 | 7.235E-02 | 3.039E-01 |
| BABEL | 7.075E-03 | 1.872E-02 | 3.417E-02 | 1.017E-01 | 2.369E-02 | 7.241E-02 | 2.920E-01 |
| PROP.-D0 | 7.103E-03 | 1.999E-02 | 3.421E-02 | 9.025E-02 | 2.358E-02 | 7.735E-02 | 3.232E-01 |
| PROP.-D1 | 6.674E-03 | 1.736E-02 | 2.816E-02 | 7.635E-02 | 2.138E-02 | 7.427E-02 | 3.165E-01 |
| EURLIB | 7.548E-03 | 2.043E-02 | 3.542E-02 | 1.064E-01 | 2.378E-02 | 7.226E-02 | 2.836E-01 |
| UKAEA | 7.278E-03 | 9.760E-03 | 1.613E-02 | 7.504E-02 | 3.083E-02 | 7.020E-02 | 2.800E-01 |
| MEAN | 7.054E-03 | 1.768E-02 | 3.041E-02 | 8.750E-02 | 2.436E-02 | 7.300E-02 | 3.004E-01 |
| ST. DEV. | 2.685E-04 | 3.353E-03 | 6.193E-03 | 1.220E-02 | 2.748E-03 | 2.073E-03 | 1.495E-02 |

TABLE 12 (Contd.) - Cr α

91080022

| DATA SET | GROUP 1 | GROUP 2 | GROUP 3 | GROUP 4 | GROUP 5 | GROUP 6 | GROUP 7 | GROUP 8 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 3.616E+00 | 3.736E+00 | 3.293E+00 | 2.943E+00 | 3.151E+00 | 3.837E+00 | 2.434E+00 | 2.351E+00 |
| VITAM.-E | 3.595E+00 | 3.733E+00 | 3.298E+00 | 2.944E+00 | 2.927E+00 | 3.841E+00 | 2.432E+00 | 2.348E+00 |
| RADHEAT | 3.633E+00 | 3.706E+00 | 3.291E+00 | 2.865E+00 | 3.340E+00 | 3.799E+00 | 2.410E+00 | 2.358E+00 |
| BABEL | 3.619E+00 | 3.709E+00 | 3.278E+00 | 2.897E+00 | 3.397E+00 | 3.848E+00 | 2.686E+00 | 2.405E+00 |
| PROP.-D0 | 3.659E+00 | 3.665E+00 | 3.219E+00 | 2.895E+00 | 3.388E+00 | 3.870E+00 | 2.676E+00 | 2.402E+00 |
| PROP.-D1 | 3.588E+00 | 3.587E+00 | 2.899E+00 | 2.792E+00 | 3.269E+00 | 3.496E+00 | 2.530E+00 | 2.288E+00 |
| EURLIB | 3.616E+00 | 3.711E+00 | 3.328E+00 | 2.923E+00 | 3.441E+00 | 3.918E+00 | 2.618E+00 | 2.404E+00 |
| UKAEA | 3.599E+00 | 3.678E+00 | 3.168E+00 | 2.874E+00 | 2.956E+00 | 3.013E+00 | 2.679E+00 | 2.029E+00 |
| MEAN | 3.616E+00 | 3.690E+00 | 3.222E+00 | 2.892E+00 | 3.233E+00 | 3.703E+00 | 2.558E+00 | 2.323E+00 |
| ST. DEV. | 2.320E-02 | 4.861E-02 | 1.399E-01 | 5.033E-02 | 2.015E-01 | 3.072E-01 | 1.208E-01 | 1.254E-01 |

TABLE 13 - Cr σ_S

320080016

| DATA SET | GROUP 9 | GROUP 10 | GROUP 11 | GROUP 12 | GROUP 13 | GROUP 14 | GROUP 15 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 4.898E+00 | 4.540E+00 | 3.016E+00 | 1.374E+01 | 4.818E+00 | 4.382E+00 | 4.344E+00 |
| VITAM.-E | 4.885E+00 | 4.603E+00 | 3.014E+00 | 1.372E+01 | 4.790E+00 | 4.377E+00 | 4.353E+00 |
| RADHEAT | 4.854E+00 | 4.517E+00 | 3.339E+00 | 1.335E+01 | 4.784E+00 | 4.371E+00 | 4.339E+00 |
| BABEL | 4.956E+00 | 4.037E+00 | 3.000E+00 | 1.388E+01 | 4.783E+00 | 4.371E+00 | 4.337E+00 |
| PROP.-D0 | 4.917E+00 | 4.031E+00 | 2.928E+00 | 1.262E+01 | 4.679E+00 | 4.372E+00 | 4.334E+00 |
| PROP.-D1 | 4.728E+00 | 3.930E+00 | 2.863E+00 | 1.241E+01 | 4.623E+00 | 4.342E+00 | 4.315E+00 |
| EURLIB | 5.667E+00 | 5.866E+00 | 3.108E+00 | 1.321E+01 | 4.784E+00 | 4.370E+00 | 4.344E+00 |
| UKAEA | 4.696E+00 | 4.359E+00 | 3.080E+00 | 9.932E+00 | 4.280E+00 | 4.265E+00 | 4.186E+00 |
| MEAN | 4.950E+00 | 4.485E+00 | 3.043E+00 | 1.286E+01 | 4.693E+00 | 4.356E+00 | 4.319E+00 |
| ST. DEV. | 3.035E-01 | 6.159E-01 | 1.426E-01 | 1.294E+00 | 1.794E-01 | 3.906E-02 | 5.520E-02 |

TABLE 13 (contd) - Cr σ_S

9108002

| DATA SET | GROUP 1 | GROUP 2 | GROUP 3 | GROUP 4 | GROUP 5 | GROUP 6 | GROUP 7 | GROUP 8 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 4.168E-01 | 1.577E-01 | 3.030E-02 | 8.606E-03 | 7.588E-03 | 7.808E-03 | 8.200E-03 | 9.073E-03 |
| VITAM.-E | 4.112E-01 | 1.599E-01 | 2.707E-02 | 8.518E-03 | 7.783E-03 | 7.792E-03 | 8.176E-03 | 8.994E-03 |
| RADHEAT | 9.906E-04 | 2.510E-03 | 5.562E-03 | 7.548E-03 | 7.536E-03 | 7.827E-03 | 8.176E-03 | 9.112E-03 |
| BABEL | 4.158E-01 | 1.459E-01 | 2.794E-02 | 8.493E-03 | 7.593E-03 | 7.847E-03 | 8.146E-03 | 8.812E-03 |
| PROP.-D0 | 3.601E-01 | 9.874E-02 | 2.122E-02 | 8.409E-03 | 7.593E-03 | 7.861E-03 | 8.159E-03 | 8.799E-03 |
| PROP.-D1 | 3.580E-01 | 9.832E-02 | 2.115E-02 | 8.359E-03 | 7.553E-03 | 7.813E-03 | 8.091E-03 | 8.706E-03 |
| EURLIB | 4.165E-01 | 1.460E-01 | 2.780E-02 | 8.478E-03 | 7.548E-03 | 7.820E-03 | 8.146E-03 | 9.067E-03 |
| UKAEA | 4.336E-01 | 1.623E-01 | 3.173E-02 | 7.573E-03 | 7.633E-03 | 7.940E-03 | 8.306E-03 | 9.196E-03 |
| MEAN | 3.516E-01 | 1.214E-01 | 2.410E-02 | 8.248E-03 | 7.604E-03 | 7.839E-03 | 8.175E-03 | 8.970E-03 |
| ST. DEV. | 1.444E-01 | 5.459E-02 | 8.405E-03 | 4.307E-04 | 7.887E-05 | 4.650E-05 | 6.238E-05 | 1.758E-04 |

TABLE 14 - Ni σ_a

| DATA SET | GROUP 9 | GROUP 10 | GROUP 11 | GROUP 12 | GROUP 13 | GROUP 14 | GROUP 15 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 1.456E-02 | 2.727E-02 | 4.543E-02 | 5.523E-02 | 3.204E-02 | 1.065E-01 | 4.440E-01 |
| VITAM.-E | 1.443E-02 | 2.711E-02 | 4.523E-02 | 5.472E-02 | 3.205E-02 | 1.063E-01 | 4.460E-01 |
| RADHEAT | 1.460E-02 | 2.619E-02 | 4.161E-02 | 5.398E-02 | 3.196E-02 | 1.058E-01 | 4.473E-01 |
| BABEL | 1.485E-02 | 2.935E-02 | 4.792E-02 | 5.790E-02 | 3.184E-02 | 1.059E-01 | 4.330E-01 |
| PROP.-D0 | 1.487E-02 | 3.051E-02 | 4.883E-02 | 5.359E-02 | 3.181E-02 | 1.132E-01 | 4.799E-01 |
| PROP.-D1 | 1.483E-02 | 3.038E-02 | 4.864E-02 | 5.350E-02 | 3.168E-02 | 1.125E-01 | 4.784E-01 |
| EURLIB | 1.455E-02 | 3.120E-02 | 5.022E-02 | 5.851E-02 | 3.196E-02 | 1.056E-01 | 4.171E-01 |
| UKAEA | 1.354E-02 | 2.741E-02 | 3.423E-02 | 5.392E-02 | 3.074E-02 | 1.005E-01 | 4.023E-01 |
| MEAN | 1.453E-02 | 2.868E-02 | 4.526E-02 | 5.517E-02 | 3.176E-02 | 1.071E-01 | 4.435E-01 |
| ST. DEV. | 4.334E-04 | 1.899E-03 | 5.221E-03 | 1.968E-03 | 4.291E-04 | 4.062E-03 | 2.690E-02 |

TABLE 14 (contd.) - Ni σ_a

1080016

| DATA SET | GROUP 1 | GROUP 2 | GROUP 3 | GROUP 4 | GROUP 5 | GROUP 6 | GROUP 7 | GROUP 8 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 3.234E+00 | 3.132E+00 | 2.979E+00 | 2.788E+00 | 3.255E+00 | 3.730E+00 | 4.562E+00 | 6.554E+00 |
| VITAM.-E | 3.273E+00 | 3.183E+00 | 3.091E+00 | 2.972E+00 | 3.269E+00 | 3.727E+00 | 4.567E+00 | 6.518E+00 |
| RADHEAT | 3.651E+00 | 3.257E+00 | 3.004E+00 | 2.845E+00 | 3.130E+00 | 3.836E+00 | 4.515E+00 | 6.592E+00 |
| BABEL | 3.236E+00 | 3.113E+00 | 2.979E+00 | 2.841E+00 | 3.203E+00 | 3.943E+00 | 4.641E+00 | 6.586E+00 |
| PROP.-D0 | 3.221E+00 | 3.069E+00 | 2.979E+00 | 2.835E+00 | 3.190E+00 | 3.957E+00 | 4.661E+00 | 6.573E+00 |
| PROP.-D1 | 3.197E+00 | 3.043E+00 | 2.904E+00 | 2.800E+00 | 3.149E+00 | 3.906E+00 | 4.531E+00 | 6.170E+00 |
| EURLIB | 3.235E+00 | 3.114E+00 | 2.987E+00 | 2.844E+00 | 3.179E+00 | 3.884E+00 | 4.588E+00 | 6.656E+00 |
| UKAEA | 3.195E+00 | 3.103E+00 | 3.279E+00 | 3.205E+00 | 3.200E+00 | 3.897E+00 | 4.618E+00 | 6.698E+00 |
| MEAN | 3.280E+00 | 3.127E+00 | 3.025E+00 | 2.891E+00 | 3.197E+00 | 3.860E+00 | 4.585E+00 | 6.543E+00 |
| ST. DEV. | 1.518E-01 | 6.688E-02 | 1.147E-01 | 1.382E-01 | 4.754E-02 | 8.922E-02 | 5.182E-02 | 1.615E-01 |

TABLE 15 - Ni σ_s

| DATA SET | GROUP 9 | GROUP 10 | GROUP 11 | GROUP 12 | GROUP 13 | GROUP 14 | GROUP 15 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 6.302E+00 | 7.862E+00 | 2.449E+01 | 2.250E+01 | 1.698E+01 | 1.777E+01 | 1.785E+01 |
| VITAM.-E | 6.274E+00 | 7.840E+00 | 2.444E+01 | 2.251E+01 | 1.692E+01 | 1.776E+01 | 1.789E+01 |
| RADHEAT | 6.281E+00 | 7.322E+00 | 2.177E+01 | 2.208E+01 | 1.689E+01 | 1.775E+01 | 1.786E+01 |
| BABEL | 6.230E+00 | 8.256E+00 | 2.649E+01 | 2.296E+01 | 1.689E+01 | 1.775E+01 | 1.785E+01 |
| PROP.-D0 | 6.208E+00 | 8.697E+00 | 2.838E+01 | 2.207E+01 | 1.699E+01 | 1.775E+01 | 1.785E+01 |
| PROP.-DI | 5.446E+00 | 8.261E+00 | 2.717E+01 | 2.143E+01 | 1.674E+01 | 1.761E+01 | 1.774E+01 |
| EURLIB | 6.386E+00 | 7.843E+00 | 2.614E+01 | 2.264E+01 | 1.689E+01 | 1.775E+01 | 1.786E+01 |
| UKAEA | 7.387E+00 | 8.937E+00 | 2.401E+01 | 2.009E+01 | 1.572E+01 | 1.720E+01 | 1.743E+01 |
| MEAN | 6.314E+00 | 8.127E+00 | 2.536E+01 | 2.204E+01 | 1.675E+01 | 1.767E+01 | 1.779E+01 |
| ST. DEV. | 5.253E-01 | 5.295E-01 | 2.090E+00 | 9.105E-01 | 4.248E-01 | 1.966E-01 | 1.543E-01 |

TABLE 15 (contd.) - Ni σ_S

9108000000

| DATA SET | GROUP 1 | GROUP 2 | GROUP 3 | GROUP 4 | GROUP 5 | GROUP 6 | GROUP 7 | GROUP 8 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 2.532E-02 | 2.177E-04 | 1.982E-04 | 2.549E-04 | 3.471E-04 | 2.792E-04 | 4.807E-04 | 6.938E-04 |
| VITAM.-E | 2.537E-02 | 2.174E-04 | 1.979E-04 | 2.538E-04 | 3.463E-04 | 3.224E-04 | 4.193E-04 | 8.297E-04 |
| RADHEAT | 1.642E-04 | 1.717E-04 | 1.986E-04 | 2.640E-04 | 3.449E-04 | 2.699E-04 | 4.727E-04 | 6.937E-04 |
| BABEL | 2.506E-02 | 2.119E-04 | 1.985E-04 | 2.636E-04 | 3.451E-04 | 2.684E-04 | 4.756E-04 | 6.939E-04 |
| PROP.-D0 | 1.749E-02 | 1.779E-04 | 2.018E-04 | 2.615E-04 | 3.449E-04 | 2.668E-04 | 4.820E-04 | 6.940E-04 |
| PROP.-D1 | 1.704E-02 | 1.766E-04 | 2.014E-04 | 2.615E-04 | 3.448E-04 | 2.661E-04 | 4.791E-04 | 6.899E-04 |
| EURLIB | 2.519E-02 | 2.113E-04 | 1.986E-04 | 2.642E-04 | 3.450E-04 | 2.703E-04 | 4.703E-04 | 6.937E-04 |
| UKAEA | 1.818E-02 | 1.410E-04 | 1.357E-04 | 2.278E-04 | 3.177E-04 | 3.980E-04 | 5.321E-04 | 6.071E-04 |
| MEAN | 1.923E-02 | 1.907E-04 | 1.913E-04 | 2.564E-04 | 3.420E-04 | 2.926E-04 | 4.765E-04 | 6.995E-04 |
| ST. DEV. | 8.592E-03 | 2.811E-05 | 2.254E-05 | 1.225E-05 | 9.850E-06 | 4.651E-05 | 3.041E-05 | 6.065E-05 |

TABLE 16 - Na in Lat. Sh. δ_{a}

| DATA SET | GROUP 9 | GROUP 10 | GROUP 11 | GROUP 12 | GROUP 13 | GROUP 14 | GROUP 15 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 9.161E-04 | 2.760E-03 | 2.308E-04 | 1.304E-02 | 8.878E-03 | 1.323E-02 | 5.191E-02 |
| VITAM.-E | 6.388E-04 | 1.934E-03 | 2.611E-05 | 9.667E-03 | 6.506E-03 | 1.278E-02 | 5.162E-02 |
| RADHEAT | 8.197E-04 | 2.484E-03 | 2.297E-04 | 1.448E-02 | 8.845E-03 | 1.318E-02 | 5.254E-02 |
| BABEL | 9.459E-04 | 2.568E-03 | 2.307E-04 | 1.192E-02 | 8.841E-03 | 1.319E-02 | 5.122E-02 |
| PROP.-D0 | 9.636E-04 | 2.299E-03 | 2.314E-04 | 1.177E-02 | 8.179E-03 | 1.406E-02 | 5.689E-02 |
| PROP.-D1 | 9.534E-04 | 2.282E-03 | 2.299E-04 | 1.167E-02 | 8.125E-03 | 1.402E-02 | 5.690E-02 |
| EURLIB | 9.221E-04 | 8.465E-03 | 2.305E-04 | 1.540E-02 | 8.855E-03 | 1.314E-02 | 4.870E-02 |
| UKAEA | 9.721E-04 | 1.598E-03 | 2.297E-03 | 1.934E-02 | 6.259E-03 | 1.278E-02 | 4.888E-02 |
| MEAN | 8.915E-04 | 3.049E-03 | 4.633E-04 | 1.341E-02 | 8.061E-03 | 1.330E-02 | 5.233E-02 |
| ST. DEV. | 1.128E-04 | 2.219E-03 | 7.445E-04 | 2.985E-03 | 1.083E-03 | 4.930E-04 | 3.133E-03 |

TABLE 16 (contd.) Na in Lat. Sh. σ_{α}

| DATA SET | GROUP 1 | GROUP 2 | GROUP 3 | GROUP 4 | GROUP 5 | GROUP 6 | GROUP 7 | GROUP 8 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 1.798E+00 | 2.262E+00 | 2.708E+00 | 4.491E+00 | 5.042E+00 | 3.040E+00 | 3.468E+00 | 3.064E+00 |
| VITAM.-E | 1.877E+00 | 2.349E+00 | 2.788E+00 | 4.619E+00 | 5.199E+00 | 3.106E+00 | 3.570E+00 | 2.932E+00 |
| RADHEAT | 1.825E+00 | 2.345E+00 | 2.704E+00 | 4.814E+00 | 4.386E+00 | 2.927E+00 | 3.505E+00 | 2.983E+00 |
| BABEL | 1.799E+00 | 2.346E+00 | 2.703E+00 | 4.808E+00 | 4.387E+00 | 2.953E+00 | 3.488E+00 | 3.076E+00 |
| PROP.-D0 | 1.905E+00 | 2.592E+00 | 2.653E+00 | 4.737E+00 | 4.380E+00 | 2.957E+00 | 3.477E+00 | 3.061E+00 |
| PROP.-D1 | 1.883E+00 | 2.556E+00 | 2.619E+00 | 4.666E+00 | 4.290E+00 | 2.893E+00 | 3.406E+00 | 2.998E+00 |
| EURLIB | 1.799E+00 | 2.348E+00 | 2.712E+00 | 4.848E+00 | 4.388E+00 | 2.957E+00 | 3.509E+00 | 3.056E+00 |
| UKAEA | 1.741E+00 | 2.365E+00 | 2.692E+00 | 5.004E+00 | 4.632E+00 | 2.992E+00 | 3.502E+00 | 3.011E+00 |
| MEAN | 1.828E+00 | 2.395E+00 | 2.697E+00 | 4.743E+00 | 4.588E+00 | 2.978E+00 | 3.491E+00 | 3.023E+00 |
| ST. DEV. | 5.540E-02 | 1.151E-01 | 4.910E-02 | 1.572E-01 | 3.455E-01 | 6.740E-02 | 4.631E-02 | 5.050E-02 |

TABLE 17 - Na in Lat. Sh. σ_s

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| DATA SET | GROUP 9 | GROUP 10 | GROUP 11 | GROUP 12 | GROUP 13 | GROUP 14 | GROUP 15 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 3.687E+00 | 4.577E+00 | 4.031E+00 | 1.381E+01 | 3.634E+00 | 3.141E+00 | 3.171E+00 |
| VITAM.-E | 3.697E+00 | 4.686E+00 | 4.215E+00 | 1.306E+01 | 3.633E+00 | 3.145E+00 | 3.172E+00 |
| RADHEAT | 3.680E+00 | 4.595E+00 | 3.983E+00 | 1.427E+01 | 3.623E+00 | 3.142E+00 | 3.160E+00 |
| BABEL | 3.668E+00 | 4.459E+00 | 4.032E+00 | 1.345E+01 | 3.623E+00 | 3.142E+00 | 3.163E+00 |
| PROP.-D0 | 3.665E+00 | 4.432E+00 | 4.054E+00 | 1.213E+01 | 3.396E+00 | 3.143E+00 | 3.170E+00 |
| PROP.-D1 | 3.550E+00 | 4.152E+00 | 3.744E+00 | 1.149E+01 | 3.209E+00 | 3.025E+00 | 3.173E+00 |
| EURLIB | 3.688E+00 | 4.923E+00 | 4.020E+00 | 1.507E+01 | 3.625E+00 | 3.142E+00 | 3.158E+00 |
| UKAEA | 3.654E+00 | 4.606E+00 | 4.184E+00 | 1.207E+01 | 3.380E+00 | 3.105E+00 | 3.160E+00 |
| MEAN | 3.661E+00 | 4.554E+00 | 4.033E+00 | 1.317E+01 | 3.515E+00 | 3.123E+00 | 3.166E+00 |
| ST. DEV. | 4.754E-02 | 2.218E-01 | 1.428E-01 | 1.222E+00 | 1.645E-01 | 4.184E-02 | 6.766E-03 |

TABLE 17 (contd.) - Na in Lat. Sh. σ_S

| DATA SET | GROUP 1 | GROUP 2 | GROUP 3 | GROUP 4 | GROUP 5 | GROUP 6 | GROUP 7 | GROUP 8 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 6.397E-02 | 2.011E-04 | 2.052E-04 | 2.664E-04 | 3.474E-04 | 2.691E-04 | 5.229E-04 | 6.938E-04 |
| VITAM.-E | 6.784E-02 | 2.023E-04 | 2.055E-04 | 2.646E-04 | 3.462E-04 | 3.175E-04 | 3.794E-04 | 4.419E-04 |
| RADHEAT | 1.685E-04 | 1.734E-04 | 2.048E-04 | 2.731E-04 | 3.439E-04 | 2.657E-04 | 5.135E-04 | 6.942E-04 |
| BABEL | 5.669E-02 | 1.957E-04 | 2.045E-04 | 2.728E-04 | 3.438E-04 | 2.646E-04 | 4.995E-04 | 6.940E-04 |
| PROP.-D0 | 3.578E-02 | 1.771E-04 | 2.045E-04 | 2.651E-04 | 3.439E-04 | 2.629E-04 | 4.923E-04 | 6.939E-04 |
| PROP.-D1 | 3.331E-02 | 1.760E-04 | 2.043E-04 | 2.651E-04 | 3.439E-04 | 2.627E-04 | 4.921E-04 | 6.924E-04 |
| EURLIB | 6.279E-02 | 1.953E-04 | 2.051E-04 | 2.739E-04 | 3.443E-04 | 2.652E-04 | 5.155E-04 | 6.937E-04 |
| UKAEA | 3.924E-02 | 1.303E-04 | 1.431E-04 | 2.372E-04 | 3.209E-04 | 4.060E-04 | 5.451E-04 | 6.071E-04 |
| MEAN | 4.498E-02 | 1.814E-04 | 1.971E-04 | 2.648E-04 | 3.418E-04 | 2.892E-04 | 4.950E-04 | 6.514E-04 |
| ST. DEV. | 2.268E-02 | 2.373E-05 | 2.183E-05 | 1.182E-05 | 8.561E-06 | 5.067E-05 | 4.993E-05 | 8.988E-05 |

TABLE 18 - Na in Na tank σ_{α}

| DATA SET | GROUP 9 | GROUP 10 | GROUP 11 | GROUP 12 | GROUP 13 | GROUP 14 | GROUP 15 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 7.282E-04 | 2.006E-03 | 2.337E-04 | 7.811E-03 | 8.517E-03 | 1.458E-02 | 9.425E-02 |
| VITAM.-E | 4.008E-04 | 1.603E-03 | 2.820E-05 | 5.897E-03 | 6.270E-03 | 1.424E-02 | 9.698E-02 |
| RADHEAT | 6.518E-04 | 1.476E-03 | 2.328E-04 | 9.151E-03 | 8.500E-03 | 1.451E-02 | 1.021E-01 |
| BABEL | 8.460E-04 | 2.677E-03 | 2.336E-04 | 7.088E-03 | 8.475E-03 | 1.455E-02 | 9.989E-02 |
| PROP.-D0 | 7.588E-04 | 2.102E-03 | 2.356E-04 | 8.114E-03 | 8.095E-03 | 1.563E-02 | 1.139E-01 |
| PROP.-D1 | 7.489E-04 | 2.098E-03 | 2.347E-04 | 8.043E-03 | 8.064E-03 | 1.541E-02 | 1.135E-01 |
| EURLIB | 8.323E-04 | 3.585E-03 | 2.334E-04 | 9.256E-03 | 8.527E-03 | 1.443E-02 | 5.904E-02 |
| UKAEA | 1.063E-03 | 1.637E-03 | 2.355E-03 | 1.502E-02 | 6.107E-03 | 1.427E-02 | 5.935E-02 |
| MEAN | 7.537E-04 | 2.148E-03 | 4.733E-04 | 8.797E-03 | 7.819E-03 | 1.470E-02 | 9.237E-02 |
| ST. DEV. | 1.874E-04 | 6.948E-04 | 7.636E-04 | 2.735E-03 | 1.025E-03 | 5.223E-04 | 2.167E-02 |

TABLE 18 (contd.) Na in Na tank σ_{α}

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| DATA SET | GROUP 1 | GROUP 2 | GROUP 3 | GROUP 4 | GROUP 5 | GROUP 6 | GROUP 7 | GROUP 8 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 1.676E+00 | 2.280E+00 | 2.590E+00 | 4.760E+00 | 4.841E+00 | 2.978E+00 | 3.359E+00 | 2.710E+00 |
| VITAM.-F | 1.747E+00 | 2.361E+00 | 2.650E+00 | 4.882E+00 | 4.978E+00 | 3.017E+00 | 3.474E+00 | 2.518E+00 |
| RADHEAT | 1.743E+00 | 2.382E+00 | 2.595E+00 | 5.016E+00 | 4.318E+00 | 2.931E+00 | 3.383E+00 | 2.731E+00 |
| BABEL | 1.695E+00 | 2.386E+00 | 2.588E+00 | 4.999E+00 | 4.303E+00 | 2.929E+00 | 3.393E+00 | 2.747E+00 |
| PROP.-D0 | 1.814E+00 | 2.544E+00 | 2.579E+00 | 4.748E+00 | 4.309E+00 | 2.926E+00 | 3.403E+00 | 2.602E+00 |
| PROP.-D1 | 1.816E+00 | 2.532E+00 | 2.569E+00 | 4.728E+00 | 4.284E+00 | 2.909E+00 | 3.379E+00 | 2.584E+00 |
| EURLIB | 1.682E+00 | 2.399E+00 | 2.634E+00 | 5.137E+00 | 4.351E+00 | 3.052E+00 | 3.398E+00 | 3.056E+00 |
| UKAEA | 1.714E+00 | 2.410E+00 | 2.671E+00 | 5.152E+00 | 4.522E+00 | 3.108E+00 | 3.398E+00 | 3.011E+00 |
| MEAN | 1.736E+00 | 2.412E+00 | 2.610E+00 | 4.928E+00 | 4.488E+00 | 2.981E+00 | 3.398E+00 | 2.745E+00 |
| ST. DEV. | 5.532E-02 | 8.733E-02 | 3.738E-02 | 1.731E-01 | 2.731E-01 | 7.166E-02 | 3.380E-02 | 1.953E-01 |

TABLE 19 - Na in Na tank σ_S

9108006

| DATA SET | GROUP 9 | GROUP 10 | GROUP 11 | GROUP 12 | GROUP 13 | GROUP 14 | GROUP 15 |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| VITAM.-C | 3.592E+00 | 4.148E+00 | 4.062E+00 | 9.356E+00 | 3.475E+00 | 3.139E+00 | 3.193E+00 |
| VITAM.-D | 3.612E+00 | 4.339E+00 | 4.244E+00 | 9.095E+00 | 3.479E+00 | 3.141E+00 | 3.200E+00 |
| RADHEAT | 3.593E+00 | 4.111E+00 | 4.043E+00 | 9.846E+00 | 3.469E+00 | 3.140E+00 | 3.200E+00 |
| BABEL | 3.587E+00 | 4.159E+00 | 4.064E+00 | 9.391E+00 | 3.459E+00 | 3.140E+00 | 3.241E+00 |
| PROP.-D0 | 3.573E+00 | 4.040E+00 | 4.111E+00 | 8.492E+00 | 3.341E+00 | 3.141E+00 | 3.263E+00 |
| PROP.-D1 | 3.493E+00 | 3.864E+00 | 3.916E+00 | 8.105E+00 | 3.177E+00 | 3.036E+00 | 3.261E+00 |
| EURLIB | 3.597E+00 | 4.569E+00 | 4.053E+00 | 1.025E+01 | 3.480E+00 | 3.140E+00 | 3.168E+00 |
| UKAEA | 3.553E+00 | 4.413E+00 | 4.212E+00 | 8.531E+00 | 3.300E+00 | 3.108E+00 | 3.171E+00 |
| MEAN | 3.575E+00 | 4.205E+00 | 4.088E+00 | 9.133E+00 | 3.397E+00 | 3.123E+00 | 3.212E+00 |
| ST. DEV. | 3.770E-02 | 2.241E-01 | 1.031E-01 | 7.270E-01 | 1.132E-01 | 3.691E-02 | 3.822E-02 |

TABLE 19 (contd.) - Na in tank σ_S 910800
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| GROUP | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 167 | | |
|-------|--------------|-----------|-----------|---------------|------------|------------|----------------|------------|------------|
| | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -6.310E-05 | 1.312E-04 | 6.809E-05 | -1.991E-05 | 3.394E-05 | 1.403E-05 | -2.110E-05 | 3.644E-05 | 1.534E-05 |
| 2 | -2.717E-04 | 6.616E-03 | 6.344E-03 | -8.628E-05 | 1.686E-03 | 1.600E-03 | -9.141E-05 | 1.812E-03 | 1.720E-03 |
| 3 | -2.433E-04 | 8.664E-03 | 8.421E-03 | -6.856E-05 | 1.758E-03 | 1.689E-03 | -7.309E-05 | 1.917E-03 | 1.844E-03 |
| 4 | -3.407E-03 | 1.198E-01 | 1.164E-01 | -8.847E-04 | 2.258E-02 | 2.170E-02 | -9.459E-04 | 2.471E-02 | 2.377E-02 |
| 5 | -2.358E-03 | 1.461E-01 | 1.438E-01 | -8.146E-04 | 3.245E-02 | 3.164E-02 | -8.607E-04 | 3.527E-02 | 3.441E-02 |
| 6 | 7.276E-04 | 1.389E-01 | 1.397E-01 | 3.056E-04 | 3.399E-02 | 3.430E-02 | 3.203E-04 | 3.683E-02 | 3.715E-02 |
| 7 | 4.223E-03 | 1.566E-01 | 1.608E-01 | 2.176E-03 | 4.143E-02 | 4.360E-02 | 2.273E-03 | 4.480E-02 | 4.707E-02 |
| 8 | 1.823E-04 | 2.192E-02 | 2.210E-02 | 4.810E-04 | 1.517E-02 | 1.565E-02 | 4.898E-04 | 1.598E-02 | 1.647E-02 |
| 9 | 0.0 | 0.0 | 0.0 | 7.884E-03 | 7.800E-02 | 8.588E-02 | 8.243E-03 | 8.486E-02 | 9.811E-02 |
| 10 | 0.0 | 0.0 | 0.0 | 4.023E-03 | 2.528E-03 | 6.551E-03 | 3.642E-03 | 2.456E-03 | 6.098E-03 |
| 11 | 0.0 | 0.0 | 0.0 | -7.948E-04 | 9.116E-03 | 8.321E-03 | -6.910E-04 | 8.438E-03 | 7.747E-03 |
| 12 | 0.0 | 0.0 | 0.0 | 5.695E-03 | -2.866E-03 | 2.830E-03 | 4.673E-03 | -2.343E-03 | 2.330E-03 |
| 13 | 0.0 | 0.0 | 0.0 | 6.143E-02 | 3.661E-03 | 6.509E-02 | 5.130E-02 | 3.711E-03 | 5.501E-02 |
| 14 | 0.0 | 0.0 | 0.0 | 5.890E-03 | 9.722E-04 | 6.863E-03 | 4.085E-03 | 6.727E-04 | 4.757E-03 |
| 15 | 0.0 | 0.0 | 0.0 | -1.491E-03 | -4.268E-05 | -1.534E-03 | -1.849E-03 | 7.466E-05 | -1.775E-03 |
| SUM | -1.211E-03 | 5.988E-01 | 5.976E-01 | 8.373E-02 | 2.405E-01 | 3.242E-01 | 7.049E-02 | 2.592E-01 | 3.297E-01 |

TABLE 20 VI - BABEL
BABEL Fe Effects

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -4.544E-04 | 1.895E-04 | -2.649E-04 | -1.434E-04 | 4.934E-05 | -9.405E-05 | -1.520E-04 | 5.293E-05 | -9.903E-05 |
| 2 | -2.335E-04 | -6.726E-04 | -9.061E-04 | -7.414E-05 | -1.705E-04 | -2.446E-04 | -7.854E-05 | -1.832E-04 | -2.618E-04 |
| 3 | -2.810E-05 | -1.913E-03 | -1.941E-03 | -7.918E-06 | -4.111E-04 | -4.190E-04 | -8.440E-06 | -4.468E-04 | -4.552E-04 |
| 4 | -1.491E-02 | -8.474E-03 | -2.339E-02 | -3.873E-03 | -1.585E-03 | -5.458E-03 | -4.141E-03 | -1.733E-03 | -5.674E-03 |
| 5 | -3.018E-03 | 7.022E-02 | 6.720E-02 | -1.043E-03 | 1.547E-02 | 1.443E-02 | -1.102E-03 | 1.683E-02 | 1.573E-02 |
| 6 | -3.954E-05 | 1.023E-03 | 9.838E-04 | -1.660E-05 | 2.502E-04 | 2.336E-04 | -1.741E-05 | 2.711E-04 | 2.537E-04 |
| 7 | 2.296E-04 | 5.527E-02 | 5.550E-02 | 1.183E-04 | 1.425E-02 | 1.437E-02 | 1.236E-04 | 1.544E-02 | 1.556E-02 |
| 8 | 3.943E-06 | 1.142E-03 | 1.146E-03 | 1.040E-05 | 8.026E-04 | 8.130E-04 | 1.059E-05 | 8.455E-04 | 8.561E-04 |
| 9 | 0.0 | 0.0 | 0.0 | 5.992E-04 | 1.170E-02 | 1.230E-02 | 6.265E-04 | 1.274E-02 | 1.337E-02 |
| 10 | 0.0 | 0.0 | 0.0 | 6.991E-05 | -8.603E-03 | -8.533E-03 | 6.329E-05 | -8.268E-03 | -8.204E-03 |
| 11 | 0.0 | 0.0 | 0.0 | 1.161E-03 | -2.784E-04 | 8.823E-04 | 1.009E-03 | -2.590E-04 | 7.502E-04 |
| 12 | 0.0 | 0.0 | 0.0 | 8.052E-03 | 8.132E-04 | 8.865E-03 | 6.606E-03 | 6.712E-04 | 7.278E-03 |
| 13 | 0.0 | 0.0 | 0.0 | -1.285E-04 | -7.861E-05 | -2.071E-04 | -1.073E-04 | -7.915E-05 | -1.865E-04 |
| 14 | 0.0 | 0.0 | 0.0 | -1.912E-04 | -8.171E-05 | -2.729E-04 | -1.326E-04 | -5.686E-05 | -1.894E-04 |
| 15 | 0.0 | 0.0 | 0.0 | -1.204E-03 | -1.887E-05 | -1.222E-03 | -1.490E-03 | 3.311E-05 | -1.457E-03 |
| SUM | -1.845E-02 | 1.168E-01 | 9.833E-02 | 3.330E-03 | 3.211E-02 | 3.544E-02 | 1.211E-03 | 3.585E-02 | 3.706E-02 |

TABLE 21 - VIT.E - BABEL Cr effects
BABEL

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| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | 4.175E-05 | -1.494E-04 | -1.077E-04 | 1.318E-05 | -3.926E-05 | -2.608E-05 | 1.396E-05 | -4.210E-05 | -2.614E-05 |
| 2 | -5.102E-04 | -1.076E-03 | -1.586E-03 | -1.620E-04 | -2.717E-04 | -4.337E-04 | -1.710E-04 | -2.923E-04 | -4.639E-04 |
| 3 | 1.220E-04 | -5.134E-03 | -5.012E-03 | 3.438E-05 | -1.115E-03 | -1.080E-03 | 3.665E-05 | -1.211E-03 | -1.174E-03 |
| 4 | -1.137E-05 | -1.151E-02 | -1.152E-02 | -2.953E-06 | -2.089E-03 | -2.092E-03 | -3.157E-06 | -2.288E-03 | -2.291E-03 |
| 5 | -4.977E-05 | -4.349E-03 | -4.399E-03 | -1.719E-05 | -9.746E-04 | -9.918E-04 | -1.816E-05 | -1.059E-03 | -1.077E-03 |
| 6 | 2.014E-05 | 1.189E-02 | 1.191E-02 | 8.458E-06 | 2.993E-03 | 3.001E-03 | 8.866E-06 | 3.234E-03 | 3.243E-03 |
| 7 | -1.210E-05 | 8.416E-03 | 8.404E-03 | -6.234E-06 | 2.156E-03 | 2.150E-03 | -6.510E-06 | 2.336E-03 | 2.329E-03 |
| 8 | -3.757E-06 | 6.921E-04 | 6.883E-04 | -9.913E-06 | 4.807E-04 | 4.708E-04 | -1.009E-05 | 5.064E-04 | 4.964E-04 |
| 9 | 0.0 | 0.0 | 0.0 | 6.022E-04 | -5.566E-03 | -4.964E-03 | 6.296E-04 | -6.086E-03 | -5.456E-03 |
| 10 | 0.0 | 0.0 | 0.0 | -5.907E-04 | 3.863E-03 | 4.453E-03 | 5.347E-04 | 3.734E-03 | 4.269E-03 |
| 11 | 0.0 | 0.0 | 0.0 | 7.310E-04 | 3.322E-02 | 3.395E-02 | 6.356E-04 | 3.125E-02 | 3.188E-02 |
| 12 | 0.0 | 0.0 | 0.0 | 8.795E-04 | 1.240E-03 | 2.120E-03 | 7.215E-04 | 1.020E-03 | 1.742E-03 |
| 13 | 0.0 | 0.0 | 0.0 | -7.451E-05 | -1.873E-04 | -2.618E-04 | -6.222E-05 | -1.886E-04 | -2.508E-04 |
| 14 | 0.0 | 0.0 | 0.0 | -1.257E-04 | -7.815E-05 | -2.038E-04 | -8.715E-05 | -5.385E-05 | -1.410E-04 |
| 15 | 0.0 | 0.0 | 0.0 | -7.082E-04 | -2.305E-05 | -7.313E-04 | -8.797E-04 | 4.067E-05 | -8.391E-04 |
| SUM | -4.033E-04 | -1.214E-03 | -1.617E-03 | 1.753E-03 | 3.361E-02 | 3.536E-02 | 1.342E-03 | 3.090E-02 | 3.224E-02 |

TABLE 22 - VIT.E BABEL Ni effects
BABEL

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| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -6.933E-06 | -7.546E-04 | -7.615E-04 | -2.186E-06 | -1.951E-04 | -1.973E-04 | -2.317E-06 | -2.094E-04 | -2.117E-04 |
| 2 | -4.978E-07 | -8.850E-05 | -8.899E-05 | -1.580E-07 | -2.261E-05 | -2.277E-05 | -1.674E-07 | -2.429E-05 | -2.445E-05 |
| 3 | 2.154E-07 | -8.732E-03 | -8.732E-03 | 6.080E-08 | -1.811E-03 | -1.811E-03 | 6.480E-08 | -1.971E-03 | -1.971E-03 |
| 4 | 1.133E-05 | 6.350E-02 | 6.351E-02 | 2.918E-06 | 1.063E-02 | 1.064E-02 | 3.122E-06 | 1.175E-02 | 1.175E-02 |
| 5 | -7.994E-07 | -2.115E-01 | -2.115E-01 | -2.630E-07 | -4.607E-02 | -4.607E-02 | -2.784E-07 | -5.026E-02 | -5.026E-02 |
| 6 | -5.307E-05 | -3.816E-02 | -3.822E-02 | -2.046E-05 | -9.180E-03 | -9.200E-03 | -2.158E-05 | -1.002E-02 | -1.004E-02 |
| 7 | 7.828E-05 | -3.439E-02 | -3.431E-02 | 2.988E-05 | -8.757E-03 | -8.728E-03 | 3.198E-05 | -9.596E-03 | -9.564E-03 |
| 8 | 7.025E-06 | 1.221E-02 | 1.222E-02 | -1.776E-05 | 3.337E-03 | 3.319E-03 | -1.672E-05 | 3.802E-03 | 3.785E-03 |
| 9 | 0.0 | 0.0 | 0.0 | 1.150E-03 | -9.678E-03 | -8.520E-03 | 1.401E-03 | -1.188E-02 | -1.048E-02 |
| 10 | 0.0 | 0.0 | 0.0 | 6.340E-04 | -6.175E-03 | -5.541E-03 | 1.096E-03 | -1.168E-02 | -1.058E-02 |
| 11 | 0.0 | 0.0 | 0.0 | 1.921E-04 | -5.007E-03 | -4.815E-03 | 2.950E-04 | -1.269E-02 | -1.240E-02 |
| 12 | 0.0 | 0.0 | 0.0 | 2.118E-03 | 3.491E-03 | 5.610E-03 | 2.914E-03 | 5.668E-03 | 8.582E-03 |
| 13 | 0.0 | 0.0 | 0.0 | 4.462E-03 | 6.141E-05 | 4.523E-03 | 1.906E-02 | -7.666E-03 | 1.139E-02 |
| 14 | 0.0 | 0.0 | 0.0 | 9.334E-04 | -4.188E-05 | 8.915E-04 | 8.411E-03 | -1.940E-03 | 6.471E-03 |
| 15 | 0.0 | 0.0 | 0.0 | 2.580E-03 | -4.648E-04 | 2.115E-03 | 6.333E-02 | 2.271E-02 | 8.605E-02 |
| SUM | 3.555E-05 | -2.179E-01 | -2.178E-01 | 1.207E-02 | -6.988E-02 | -5.781E-02 | 9.651E-02 | -7.402E-02 | 2.249E-02 |

TABLE 23 - VIT.E - BABEL
BABEL

Na effects

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| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -4.827E-04 | -5.833E-04 | -1.066E-03 | -1.523E-04 | -1.511E-04 | -3.034E-04 | -1.614E-04 | -1.621E-04 | -3.235E-04 |
| 2 | -1.016E-03 | 4.779E-03 | 3.763E-03 | -3.226E-04 | 1.221E-03 | 8.986E-04 | -3.418E-04 | 1.312E-03 | 9.702E-04 |
| 3 | -1.492E-04 | -7.115E-03 | -7.264E-03 | -4.204E-05 | -1.579E-03 | -1.621E-03 | -4.482E-05 | -1.711E-03 | -1.756E-03 |
| 4 | -1.832E-02 | 1.634E-01 | 1.450E-01 | -4.758E-03 | 2.955E-02 | 2.479E-02 | -5.087E-03 | 3.244E-02 | 2.735E-02 |
| 5 | -5.427E-03 | 5.455E-04 | -4.882E-03 | -1.875E-03 | 8.719E-04 | -1.003E-03 | -1.981E-03 | 7.794E-04 | -1.201E-03 |
| 6 | 6.551E-04 | 1.137E-01 | 1.144E-01 | 2.770E-04 | 2.806E-02 | 2.833E-02 | 2.902E-04 | 3.031E-02 | 3.061E-02 |
| 7 | 4.518E-03 | 1.859E-01 | 1.904E-01 | 2.318E-03 | 4.908E-02 | 5.140E-02 | 2.422E-03 | 5.297E-02 | 5.540E-02 |
| 8 | 1.895E-04 | 3.597E-02 | 3.616E-02 | 4.637E-04 | 1.979E-02 | 2.025E-02 | 4.736E-04 | 2.113E-02 | 2.161E-02 |
| 9 | 0.0 | 0.0 | 0.0 | 1.024E-02 | 7.446E-02 | 8.470E-02 | 1.090E-02 | 7.963E-02 | 9.053E-02 |
| 10 | 0.0 | 0.0 | 0.0 | 5.318E-03 | -8.388E-03 | -3.070E-03 | 5.336E-03 | -1.376E-02 | -8.419E-03 |
| 11 | 0.0 | 0.0 | 0.0 | 1.289E-03 | 3.705E-02 | 3.834E-02 | 1.249E-03 | 2.673E-02 | 2.796E-02 |
| 12 | 0.0 | 0.0 | 0.0 | 1.675E-02 | 2.679E-03 | 1.942E-02 | 1.492E-02 | 5.016E-03 | 1.993E-02 |
| 13 | 0.0 | 0.0 | 0.0 | 6.569E-02 | 3.456E-03 | 6.915E-02 | 7.019E-02 | -4.223E-03 | 6.597E-02 |
| 14 | 0.0 | 0.0 | 0.0 | 6.507E-03 | 7.705E-04 | 7.277E-03 | 1.228E-02 | -1.378E-03 | 1.090E-02 |
| 15 | 0.0 | 0.0 | 0.0 | -8.230E-04 | -5.494E-04 | -1.372E-03 | 5.911E-02 | 2.286E-02 | 8.198E-02 |
| SUM | -2.003E-02 | 4.965E-01 | 4.765E-01 | 1.009E-01 | 2.363E-01 | 3.372E-01 | 1.695E-01 | 2.520E-01 | 4.215E-01 |

TABLE 24 - VIT.E - BABEL
BABEL Total effects

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|-----------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | 2.849E-03 | -1.297E-03 | 1.552E-03 | 8.991E-04 | -3.356E-04 | 5.634E-04 | 9.527E-04 | -3.603E-04 | 5.924E-04 |
| 2 | 2.399E-03 | 9.306E-04 | 3.330E-03 | 7.619E-04 | 2.371E-04 | 9.990E-04 | 8.072E-04 | 2.548E-04 | 1.062E-03 |
| 3 | 8.672E-04 | 2.525E-02 | 2.612E-02 | 2.443E-04 | 5.123E-03 | 5.367E-03 | 2.605E-04 | 5.588E-03 | 5.848E-03 |
| 4 | 1.741E-06 | 1.597E-01 | 1.597E-01 | 4.520E-07 | 3.010E-02 | 3.010E-02 | 4.833E-07 | 3.294E-02 | 3.294E-02 |
| 5 | 3.161E-06 | 9.497E-02 | 9.498E-02 | 1.092E-06 | 2.109E-02 | 2.109E-02 | 1.154E-06 | 2.292E-02 | 2.293E-02 |
| 6 | -1.102E-05 | 1.099E-01 | 1.099E-01 | -4.629E-06 | 2.688E-02 | 2.688E-02 | -4.853E-06 | 2.912E-02 | 2.912E-02 |
| 7 | -1.837E-05 | 1.480E-01 | 1.480E-01 | -9.465E-06 | 3.915E-02 | 3.914E-02 | -9.884E-06 | 4.234E-02 | 4.233E-02 |
| 8 | -5.162E-07 | 1.309E-02 | 1.309E-02 | -1.362E-06 | 9.056E-03 | 9.055E-03 | -1.387E-06 | 9.542E-03 | 9.541E-03 |
| 9 | 0.0 | 0.0 | 0.0 | -1.309E-03 | 4.694E-03 | 3.386E-03 | -1.368E-03 | 5.108E-03 | 3.739E-03 |
| 10 | 0.0 | 0.0 | 0.0 | 8.010E-03 | -5.679E-03 | 2.332E-03 | 7.252E-03 | -5.519E-03 | 1.733E-03 |
| 11 | 0.0 | 0.0 | 0.0 | -1.106E-03 | -1.329E-01 | -1.340E-01 | -9.616E-04 | -1.230E-01 | -1.240E-01 |
| 12 | 0.0 | 0.0 | 0.0 | 1.721E-03 | -3.682E-03 | -1.961E-03 | 1.412E-03 | -3.011E-03 | -1.599E-03 |
| 13 | 0.0 | 0.0 | 0.0 | 6.068E-02 | 3.577E-05 | 6.072E-02 | 5.067E-02 | 3.627E-05 | 5.071E-02 |
| 14 | 0.0 | 0.0 | 0.0 | 1.469E-04 | 2.276E-05 | 1.697E-04 | 1.019E-04 | 1.575E-05 | 1.176E-04 |
| 15 | 0.0 | 0.0 | 0.0 | -1.504E-03 | -4.266E-06 | -1.508E-03 | -1.865E-03 | 7.463E-06 | -1.857E-03 |
| SUM | 6.091E-03 | 5.505E-01 | 5.566E-01 | 6.853E-02 | -6.243E-03 | 6.229E-02 | 5.725E-02 | 1.594E-02 | 7.319E-02 |

TABLE 25 - RADHEAT-BABEL
BABEL

0108000

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | 2.499E-04 | -1.099E-04 | 1.400E-04 | 7.887E-05 | -2.861E-05 | 5.026E-05 | 8.358E-05 | -3.069E-05 | 5.289E-05 |
| 2 | 1.050E-04 | 9.573E-05 | 2.007E-04 | 3.334E-05 | 2.426E-05 | 5.760E-05 | 3.532E-05 | 2.608E-05 | 6.140E-05 |
| 3 | 8.107E-06 | -1.257E-03 | -1.249E-03 | 2.284E-06 | -2.701E-04 | -2.678E-04 | 2.435E-06 | -2.935E-04 | -2.911E-04 |
| 4 | 5.428E-06 | 5.727E-03 | 5.732E-03 | 1.410E-06 | 1.071E-03 | 1.072E-03 | 1.507E-06 | 1.171E-03 | 1.173E-03 |
| 5 | 4.906E-05 | 8.589E-03 | 8.638E-03 | 1.694E-05 | 1.892E-03 | 1.909E-03 | 1.790E-05 | 2.058E-03 | 2.076E-03 |
| 6 | 1.318E-05 | 6.945E-03 | 6.958E-03 | 5.535E-06 | 1.698E-03 | 1.704E-03 | 5.802E-06 | 1.840E-03 | 1.846E-03 |
| 7 | 2.092E-04 | 6.004E-02 | 6.025E-02 | 1.078E-04 | 1.548E-02 | 1.559E-02 | 1.126E-04 | 1.677E-02 | 1.688E-02 |
| 8 | 1.017E-06 | 9.463E-04 | 9.474E-04 | 2.684E-06 | 6.649E-04 | 6.675E-04 | 2.733E-06 | 7.004E-04 | 7.031E-04 |
| 9 | 0.0 | 0.0 | 0.0 | 5.145E-04 | 1.683E-02 | 1.735E-02 | 5.379E-04 | 1.833E-02 | 1.886E-02 |
| 10 | 0.0 | 0.0 | 0.0 | 4.082E-04 | -7.297E-03 | -6.889E-03 | 3.695E-04 | -7.013E-03 | -6.644E-03 |
| 11 | 0.0 | 0.0 | 0.0 | 1.711E-03 | -6.499E-03 | -4.788E-03 | 1.487E-03 | -6.045E-03 | -4.558E-03 |
| 12 | 0.0 | 0.0 | 0.0 | 1.576E-02 | 2.728E-03 | 1.849E-02 | 1.293E-02 | 2.251E-03 | 1.518E-02 |
| 13 | 0.0 | 0.0 | 0.0 | -6.318E-05 | -2.023E-05 | -8.341E-05 | -5.276E-05 | -2.037E-05 | -7.312E-05 |
| 14 | 0.0 | 0.0 | 0.0 | 5.112E-05 | -2.041E-06 | 4.908E-05 | 3.545E-05 | -1.420E-06 | 3.403E-05 |
| 15 | 0.0 | 0.0 | 0.0 | -1.321E-03 | -2.973E-06 | -1.324E-03 | -1.635E-03 | 5.217E-06 | -1.630E-03 |
| SUM | 6.409E-04 | 8.098E-02 | 8.162E-02 | 1.731E-02 | 2.628E-02 | 4.359E-02 | 1.394E-02 | 2.974E-02 | 4.368E-02 |

TABLE 26 ~ RADHEAT-BABEL
BABEL

Cr effects

910800

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | 3.717E-03 | -1.691E-03 | 2.026E-03 | 1.173E-03 | -4.443E-04 | 7.286E-04 | 1.243E-03 | -4.765E-04 | 7.664E-04 |
| 2 | 5.214E-03 | -2.226E-03 | 2.988E-03 | 1.656E-03 | -5.622E-04 | 1.093E-03 | 1.754E-03 | -6.049E-04 | 1.149E-03 |
| 3 | 3.152E-03 | -1.136E-03 | 2.016E-03 | 8.882E-04 | -2.467E-04 | 6.415E-04 | 9.468E-04 | -2.679E-04 | 6.789E-04 |
| 4 | 4.351E-04 | -3.759E-04 | 5.926E-05 | 1.130E-04 | -6.823E-05 | 4.477E-05 | 1.208E-04 | -7.475E-05 | 4.607E-05 |
| 5 | 1.469E-05 | 4.825E-03 | 4.839E-03 | 5.073E-06 | 1.081E-03 | 1.086E-03 | 5.360E-06 | 1.174E-03 | 1.180E-03 |
| 6 | 7.537E-06 | 5.885E-03 | 5.892E-03 | 3.166E-06 | 1.481E-03 | 1.484E-03 | 3.318E-06 | 1.600E-03 | 1.604E-03 |
| 7 | -1.230E-05 | 1.437E-02 | 1.436E-02 | -6.341E-06 | 3.683E-03 | 3.676E-03 | -6.621E-06 | 3.990E-03 | 3.983E-03 |
| 8 | -6.203E-06 | -6.859E-05 | -7.479E-05 | -1.637E-05 | -4.764E-05 | -6.401E-05 | -1.667E-05 | -5.020E-05 | -6.686E-05 |
| 9 | 0.0 | 0.0 | 0.0 | 3.627E-04 | -6.395E-03 | -6.032E-03 | 3.793E-04 | -6.992E-03 | -6.612E-03 |
| 10 | 0.0 | 0.0 | 0.0 | 8.343E-04 | 8.669E-03 | 9.503E-03 | 7.553E-04 | 8.380E-03 | 9.135E-03 |
| 11 | 0.0 | 0.0 | 0.0 | 1.714E-03 | 7.642E-02 | 7.813E-02 | 1.491E-03 | 7.189E-02 | 7.338E-02 |
| 12 | 0.0 | 0.0 | 0.0 | 1.085E-03 | 2.468E-03 | 3.552E-03 | 8.898E-04 | 2.030E-03 | 2.920E-03 |
| 13 | 0.0 | 0.0 | 0.0 | -4.202E-05 | 6.725E-06 | -3.530E-05 | -3.509E-05 | 6.771E-06 | -2.832E-05 |
| 14 | 0.0 | 0.0 | 0.0 | 3.427E-05 | 2.137E-06 | 3.641E-05 | 2.377E-05 | 1.473E-06 | 2.524E-05 |
| 15 | 0.0 | 0.0 | 0.0 | -7.745E-04 | -3.929E-06 | -7.784E-04 | -9.620E-04 | 6.931E-06 | -9.551E-04 |
| SUM | 1.252E-02 | 1.959E-02 | 3.211E-02 | 7.029E-03 | 8.604E-02 | 9.307E-02 | 6.591E-03 | 8.061E-02 | 8.720E-02 |

TABLE 27 - RADHEAT-BABEL Ni effects
BABEL

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | 5.511E-04 | -2.464E-04 | 3.046E-04 | 1.739E-04 | -6.372E-05 | 1.102E-04 | 1.843E-04 | -6.838E-05 | 1.159E-04 |
| 2 | 3.613E-06 | 3.066E-05 | 3.427E-05 | 1.147E-06 | 7.840E-06 | 8.987E-06 | 1.215E-06 | 8.423E-06 | 9.638E-06 |
| 3 | -4.191E-08 | -1.241E-04 | -1.241E-04 | -1.177E-08 | -2.590E-05 | -2.592E-05 | -1.255E-08 | -2.823E-05 | -2.824E-05 |
| 4 | -3.673E-07 | -2.113E-03 | -2.113E-03 | -9.456E-08 | -3.565E-04 | -3.566E-04 | -1.012E-07 | -3.943E-04 | -3.944E-04 |
| 5 | 1.218E-07 | 2.335E-04 | 2.336E-04 | 4.228E-08 | 4.655E-05 | 4.660E-05 | 4.467E-08 | 5.019E-05 | 5.024E-05 |
| 6 | -1.420E-06 | 6.701E-03 | 6.699E-03 | -5.602E-07 | 1.584E-03 | 1.584E-03 | -5.898E-07 | 1.721E-03 | 1.720E-03 |
| 7 | 5.422E-07 | -7.512E-03 | -7.511E-03 | 1.499E-06 | -1.896E-03 | -1.895E-03 | 1.475E-06 | -2.044E-03 | -2.043E-03 |
| 8 | 1.300E-09 | 3.940E-03 | 3.940E-03 | 2.794E-08 | 2.180E-03 | 2.180E-03 | 2.753E-08 | 2.320E-03 | 2.320E-03 |
| 9 | 0.0 | 0.0 | 0.0 | 4.780E-04 | -4.040E-03 | -3.562E-03 | 5.827E-04 | -4.728E-03 | -4.145E-03 |
| 10 | 0.0 | 0.0 | 0.0 | 3.003E-04 | -4.219E-03 | -3.919E-03 | 8.555E-04 | -2.602E-03 | -1.747E-03 |
| 11 | 0.0 | 0.0 | 0.0 | 9.354E-07 | 1.493E-03 | 1.494E-03 | 1.337E-06 | 2.329E-03 | 2.330E-03 |
| 12 | 0.0 | 0.0 | 0.0 | -2.753E-03 | -7.406E-03 | -1.016E-02 | -4.297E-03 | -1.039E-02 | -1.468E-02 |
| 13 | 0.0 | 0.0 | 0.0 | -3.178E-05 | 1.324E-04 | 1.006E-04 | -2.003E-04 | -3.706E-03 | -3.906E-03 |
| 14 | 0.0 | 0.0 | 0.0 | 7.959E-05 | -3.213E-06 | 7.638E-05 | 1.050E-03 | -2.693E-04 | 7.809E-04 |
| 15 | 0.0 | 0.0 | 0.0 | -2.163E-03 | -4.398E-04 | -2.603E-03 | -4.927E-02 | 2.208E-02 | -2.719E-02 |
| SUM | 5.535E-04 | 9.095E-04 | 1.463E-03 | -3.913E-03 | -1.301E-02 | -1.692E-02 | -5.109E-02 | 4.281E-03 | -4.681E-02 |

TABLE 28 - RADHEAT-BABEL
BABEL Na effects

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|-----------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | 7.367E-03 | -3.345E-03 | 4.022E-03 | 2.325E-03 | -8.723E-04 | 1.452E-03 | 2.463E-03 | -9.358E-04 | 1.528E-03 |
| 2 | 7.722E-03 | -1.169E-03 | 6.553E-03 | 2.452E-03 | -2.930E-04 | 2.159E-03 | 2.598E-03 | -3.155E-04 | 2.282E-03 |
| 3 | 4.028E-03 | 2.273E-02 | 2.676E-02 | 1.135E-03 | 4.580E-03 | 5.715E-03 | 1.210E-03 | 4.998E-03 | 6.208E-03 |
| 4 | 4.419E-04 | 1.630E-01 | 1.634E-01 | 1.148E-04 | 3.075E-02 | 3.086E-02 | 1.227E-04 | 3.364E-02 | 3.376E-02 |
| 5 | 6.702E-05 | 1.086E-01 | 1.087E-01 | 2.315E-05 | 2.411E-02 | 2.413E-02 | 2.446E-05 | 2.621E-02 | 2.623E-02 |
| 6 | 8.274E-06 | 1.294E-01 | 1.294E-01 | 3.511E-06 | 3.164E-02 | 3.165E-02 | 3.678E-06 | 3.428E-02 | 3.429E-02 |
| 7 | 1.791E-04 | 2.149E-01 | 2.151E-01 | 9.351E-05 | 5.642E-02 | 5.652E-02 | 9.756E-05 | 6.105E-02 | 6.115E-02 |
| 8 | -5.700E-06 | 1.791E-02 | 1.790E-02 | -1.502E-05 | 1.185E-02 | 1.184E-02 | -1.529E-05 | 1.251E-02 | 1.250E-02 |
| 9 | 0.0 | 0.0 | 0.0 | 4.645E-05 | 1.109E-02 | 1.114E-02 | 1.315E-04 | 1.171E-02 | 1.184E-02 |
| 10 | 0.0 | 0.0 | 0.0 | 9.553E-03 | -8.526E-03 | 1.027E-03 | 9.232E-03 | -6.754E-03 | 2.478E-03 |
| 11 | 0.0 | 0.0 | 0.0 | 2.320E-03 | -6.152E-02 | -5.920E-02 | 2.017E-03 | -5.487E-02 | -5.286E-02 |
| 12 | 0.0 | 0.0 | 0.0 | 1.582E-02 | -5.893E-03 | 9.923E-03 | 1.094E-02 | -9.114E-03 | 1.823E-03 |
| 13 | 0.0 | 0.0 | 0.0 | 6.055E-02 | 1.547E-04 | 6.070E-02 | 5.038E-02 | -3.683E-03 | 4.670E-02 |
| 14 | 0.0 | 0.0 | 0.0 | 3.119E-04 | 1.964E-05 | 3.315E-04 | 1.211E-03 | -2.535E-04 | 9.578E-04 |
| 15 | 0.0 | 0.0 | 0.0 | -5.762E-03 | -4.510E-04 | -6.213E-03 | -5.373E-02 | 2.210E-02 | -3.164E-02 |
| SUM | 1.981E-02 | 6.520E-01 | 6.718E-01 | 8.896E-02 | 9.307E-02 | 1.820E-01 | 2.668E-02 | 1.306E-01 | 1.573E-01 |

TABLE 29 - RADHEAT-BABEL
BABEL Total effects

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|-----------|-----------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -5.205E-05 | 1.165E-04 | 6.445E-05 | -1.643E-05 | 3.014E-05 | 1.372E-05 | -1.741E-05 | 3.236E-05 | 1.495E-05 |
| 2 | -2.285E-04 | 6.619E-03 | 6.390E-03 | -7.257E-05 | 1.687E-03 | 1.614E-03 | -7.688E-05 | 1.813E-03 | 1.736E-03 |
| 3 | -1.375E-04 | 1.078E-02 | 1.064E-02 | -3.874E-05 | 2.187E-03 | 2.148E-03 | -4.130E-05 | 2.385E-03 | 2.344E-03 |
| 4 | 5.658E-04 | 1.286E-01 | 1.291E-01 | 1.469E-04 | 2.423E-02 | 2.437E-02 | 1.571E-04 | 2.651E-02 | 2.667E-02 |
| 5 | -2.388E-05 | 1.466E-01 | 1.465E-01 | -8.247E-06 | 3.255E-02 | 3.254E-02 | -8.714E-06 | 3.538E-02 | 3.537E-02 |
| 6 | -6.199E-05 | 1.431E-01 | 1.430E-01 | -2.603E-05 | 3.500E-02 | 3.498E-02 | -2.729E-05 | 3.793E-02 | 3.790E-02 |
| 7 | -1.774E-05 | 1.640E-01 | 1.640E-01 | -9.143E-06 | 4.340E-02 | 4.339E-02 | -9.547E-06 | 4.693E-02 | 4.692E-02 |
| 8 | -7.353E-07 | 7.565E-03 | 7.565E-03 | -1.940E-06 | 5.234E-03 | 5.232E-03 | -1.976E-06 | 5.515E-03 | 5.513E-03 |
| 9 | 0.0 | 0.0 | 0.0 | 1.061E-04 | 2.516E-02 | 2.527E-02 | 1.109E-04 | 2.737E-02 | 2.748E-02 |
| 10 | 0.0 | 0.0 | 0.0 | 2.713E-03 | 1.820E-03 | 4.533E-03 | 2.456E-03 | 1.769E-03 | 4.225E-03 |
| 11 | 0.0 | 0.0 | 0.0 | 9.243E-04 | 1.124E-02 | 1.217E-02 | 8.036E-04 | 1.041E-02 | 1.121E-02 |
| 12 | 0.0 | 0.0 | 0.0 | 3.554E-04 | -3.892E-03 | -3.537E-03 | 2.916E-04 | -3.182E-03 | -2.891E-03 |
| 13 | 0.0 | 0.0 | 0.0 | 3.964E-02 | -1.173E-04 | 3.953E-02 | 3.310E-02 | -1.189E-04 | 3.299E-02 |
| 14 | 0.0 | 0.0 | 0.0 | -6.999E-04 | 4.049E-05 | -6.595E-04 | -4.854E-04 | 2.801E-05 | -4.574E-04 |
| 15 | 0.0 | 0.0 | 0.0 | -1.265E-03 | 0.0 | -1.265E-03 | -1.569E-03 | 0.0 | -1.569E-03 |
| SUM | 4.338E-05 | 6.073E-01 | 6.074E-01 | 4.175E-02 | 1.786E-01 | 2.203E-01 | 3.469E-02 | 1.928E-01 | 2.275E-01 |

TABLE 30 - VIT.C-BABEL
BABEL Fe effects

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -3.871E-05 | 2.262E-05 | -1.609E-05 | +1.222E-05 | 5.889E-06 | -6.326E-06 | -1.294E-05 | 6.317E-06 | -6.627E-06 |
| 2 | -7.238E-06 | -7.625E-04 | -7.698E-04 | -2.298E-06 | -1.933E-04 | -1.956E-04 | -2.435E-06 | -2.077E-04 | -2.102E-04 |
| 3 | 2.303E-05 | -1.433E-03 | -1.409E-03 | 6.489E-06 | -3.078E-04 | -3.013E-04 | 6.918E-06 | -3.345E-04 | -3.276E-04 |
| 4 | -9.563E-05 | -8.368E-03 | -8.464E-03 | -2.484E-05 | -1.565E-03 | -1.590E-03 | -2.655E-05 | -1.711E-03 | -1.738E-03 |
| 5 | -1.337E-04 | 3.683E-02 | 3.670E-02 | +4.618E-05 | 8.114E-03 | 8.068E-03 | -4.879E-05 | 8.826E-03 | 8.778E-03 |
| 6 | -4.790E-05 | 1.595E-03 | 1.547E-03 | -2.012E-05 | 3.899E-04 | 3.698E-04 | -2.109E-05 | 4.224E-04 | 4.013E-04 |
| 7 | 2.227E-04 | 5.491E-02 | 5.513E-02 | 1.148E-04 | 1.416E-02 | 1.428E-02 | 1.199E-04 | 1.534E-02 | 1.546E-02 |
| 8 | 2.892E-06 | 1.075E-03 | 1.078E-03 | 7.631E-06 | 7.555E-04 | 7.631E-04 | 7.771E-06 | 7.958E-04 | 8.036E-04 |
| 9 | 0.0 | 0.0 | 0.0 | 2.420E-04 | 9.509E-03 | 9.751E-03 | 2.530E-04 | 1.035E-02 | 1.060E-02 |
| 10 | 0.0 | 0.0 | 0.0 | 2.958E-05 | -7.647E-03 | -7.618E-03 | 2.678E-05 | -7.350E-03 | -7.323E-03 |
| 11 | 0.0 | 0.0 | 0.0 | 1.157E-03 | -3.181E-04 | 8.388E-04 | 1.006E-03 | -2.959E-04 | 7.100E-04 |
| 12 | 0.0 | 0.0 | 0.0 | 6.925E-03 | 7.241E-04 | 7.649E-03 | 5.682E-03 | 5.977E-04 | 6.279E-03 |
| 13 | 0.0 | 0.0 | 0.0 | -1.960E-04 | -3.910E-04 | -5.870E-04 | -1.637E-04 | -3.937E-04 | -5.573E-04 |
| 14 | 0.0 | 0.0 | 0.0 | -9.597E-05 | -1.412E-04 | -2.371E-04 | -6.654E-05 | -9.823E-05 | -1.648E-04 |
| 15 | 0.0 | 0.0 | 0.0 | -9.927E-04 | -9.035E-06 | -1.002E-03 | -1.229E-03 | 1.585E-05 | -1.213E-03 |
| SUM | -7.450E-05 | 8.387E-02 | 8.380E-02 | 7.092E-03 | 2.309E-02 | 3.018E-02 | 5.531E-03 | 2.596E-02 | 3.149E-02 |

TABLE 31 - VIT.C-BABEL
BABEL Cr effects

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -8.422E-06 | 9.242E-06 | 8.199E-07 | -2.658E-06 | 2.428E-06 | -2.296E-07 | -2.816E-06 | 2.604E-06 | -2.125E-07 |
| 2 | -4.302E-04 | -2.911E-04 | -7.213E-04 | -1.366E-04 | -7.352E-05 | -2.101E-04 | -1.447E-04 | -7.910E-05 | -2.238E-04 |
| 3 | -3.335E-04 | 1.529E-05 | -3.182E-04 | -9.397E-05 | 3.319E-06 | -9.065E-05 | -1.002E-04 | 3.604E-06 | -9.656E-05 |
| 4 | -5.206E-05 | 4.620E-03 | 4.568E-03 | -1.352E-05 | 8.387E-04 | 8.252E-04 | -1.445E-05 | 9.188E-04 | 9.043E-04 |
| 5 | 1.148E-06 | -3.426E-03 | -3.425E-03 | 3.964E-07 | -7.677E-04 | -7.673E-04 | 4.188E-07 | -8.338E-04 | -8.334E-04 |
| 6 | 1.435E-05 | 1.169E-02 | 1.170E-02 | 6.026E-06 | 2.940E-03 | 2.946E-03 | 6.317E-06 | 3.178E-03 | 3.184E-03 |
| 7 | -2.201E-05 | 9.007E-03 | 8.985E-03 | -1.134E-05 | 2.308E-03 | 2.296E-03 | -1.185E-05 | 2.500E-03 | 2.488E-03 |
| 8 | -5.402E-06 | 3.225E-04 | 3.171E-04 | -1.426E-05 | 2.240E-04 | 2.098E-04 | -1.452E-05 | 2.360E-04 | 2.215E-04 |
| 9 | 0.0 | 0.0 | 0.0 | 4.222E-04 | -9.014E-03 | -8.592E-03 | 4.415E-04 | -9.856E-03 | -9.414E-03 |
| 10 | 0.0 | 0.0 | 0.0 | 5.481E-04 | 3.653E-03 | 4.202E-03 | 4.962E-04 | 3.532E-03 | 4.028E-03 |
| 11 | 0.0 | 0.0 | 0.0 | 6.756E-04 | 3.230E-02 | 3.298E-02 | 5.874E-04 | 3.039E-02 | 3.098E-02 |
| 12 | 0.0 | 0.0 | 0.0 | 7.385E-04 | 1.282E-03 | 2.021E-03 | 6.059E-04 | 1.055E-03 | 1.661E-03 |
| 13 | 0.0 | 0.0 | 0.0 | -7.346E-05 | -4.893E-04 | -5.627E-04 | -6.134E-05 | -4.926E-04 | -5.540E-04 |
| 14 | 0.0 | 0.0 | 0.0 | -2.323E-04 | -1.300E-04 | -3.623E-04 | -1.611E-04 | -8.962E-05 | -2.507E-04 |
| 15 | 0.0 | 0.0 | 0.0 | -5.963E-04 | -1.681E-06 | -5.980E-04 | -7.407E-04 | 2.966E-06 | -7.378E-04 |
| SUM | -8.361E-04 | 2.194E-02 | 2.111E-02 | 1.216E-03 | 3.308E-02 | 3.429E-02 | 8.859E-04 | 3.047E-02 | 3.135E-02 |

TABLE 32 - VIT.C-BABEL
BABEL Ni effects

0000016

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -5.824E-06 | 1.321E-05 | 7.387E-06 | -1.837E-06 | 3.417E-06 | 1.580E-06 | -1.947E-06 | 3.667E-06 | 1.720E-06 |
| 2 | -5.220E-07 | 2.865E-03 | 2.864E-03 | -1.657E-07 | 7.323E-04 | 7.322E-04 | -1.756E-07 | 7.868E-04 | 7.866E-04 |
| 3 | 9.720E-08 | -5.654E-04 | -5.653E-04 | 2.746E-08 | -1.172E-04 | -1.172E-04 | 2.926E-08 | -1.276E-04 | -1.276E-04 |
| 4 | 1.003E-05 | 1.068E-01 | 1.069E-01 | 2.587E-06 | 1.790E-02 | 1.791E-02 | 2.767E-06 | 1.978E-02 | 1.978E-02 |
| 5 | -1.361E-06 | -1.705E-01 | -1.705E-01 | -4.501E-07 | -3.714E-02 | -3.714E-02 | -4.765E-07 | -4.052E-02 | -4.052E-02 |
| 6 | -1.011E-05 | -2.168E-02 | -2.169E-02 | -4.092E-06 | -5.215E-03 | -5.219E-03 | -4.301E-06 | -5.693E-03 | -5.697E-03 |
| 7 | -9.270E-06 | 8.163E-03 | 8.154E-03 | -2.736E-06 | 2.088E-03 | 2.085E-03 | -3.008E-06 | 2.306E-03 | 2.303E-03 |
| 8 | 1.662E-08 | 1.564E-03 | 1.564E-03 | 1.793E-08 | 2.771E-04 | 2.771E-04 | 1.923E-08 | 3.381E-04 | 3.381E-04 |
| 9 | 0.0 | 0.0 | 0.0 | 1.263E-04 | -6.460E-03 | -6.334E-03 | 1.824E-04 | -7.323E-03 | -7.141E-03 |
| 10 | 0.0 | 0.0 | 0.0 | 1.143E-05 | -3.550E-03 | -3.539E-03 | 3.365E-04 | -3.100E-03 | -2.764E-03 |
| 11 | 0.0 | 0.0 | 0.0 | -6.564E-08 | 1.175E-05 | 1.168E-05 | -1.007E-07 | 9.109E-05 | 9.099E-05 |
| 12 | 0.0 | 0.0 | 0.0 | -1.113E-03 | -3.276E-03 | -4.389E-03 | -1.628E-03 | -2.344E-03 | -3.972E-03 |
| 13 | 0.0 | 0.0 | 0.0 | -7.945E-05 | -1.437E-05 | -9.382E-05 | -3.640E-04 | -5.984E-03 | -6.348E-03 |
| 14 | 0.0 | 0.0 | 0.0 | -8.407E-05 | 2.486E-06 | -8.158E-05 | -6.669E-04 | 1.450E-03 | 7.832E-04 |
| 15 | 0.0 | 0.0 | 0.0 | 4.999E-03 | -5.373E-04 | 4.462E-03 | 1.225E-01 | 2.640E-02 | 1.489E-01 |
| SUM | -1.694E-05 | -7.327E-02 | -7.329E-02 | 3.854E-03 | -3.529E-02 | -3.144E-02 | 1.204E-01 | -1.394E-02 | 1.064E-01 |

TABLE 33 - VIT.C-BABEG
BABEL

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| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|-----------|-----------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -1.050E-04 | 1.616E-04 | 5.657E-05 | -3.314E-05 | 4.188E-05 | 8.741E-06 | -3.511E-05 | 4.495E-05 | 9.831E-06 |
| 2 | -6.665E-04 | 8.430E-03 | 7.764E-03 | -2.116E-04 | 2.152E-03 | 1.941E-03 | -2.242E-04 | 2.313E-03 | 2.088E-03 |
| 3 | -4.479E-04 | 8.796E-03 | 8.348E-03 | -1.262E-04 | 1.765E-03 | 1.639E-03 | -1.345E-04 | 1.927E-03 | 1.792E-03 |
| 4 | 4.282E-04 | 2.317E-01 | 2.321E-01 | 1.112E-04 | 4.140E-02 | 4.151E-02 | 1.189E-04 | 4.550E-02 | 4.562E-02 |
| 5 | -1.578E-04 | 9.503E-03 | 9.345E-03 | -5.448E-05 | 2.752E-03 | 2.697E-03 | -5.756E-05 | 2.852E-03 | 2.795E-03 |
| 6 | -1.057E-04 | 1.347E-01 | 1.346E-01 | -4.422E-05 | 3.312E-02 | 3.308E-02 | -4.637E-05 | 3.583E-02 | 3.579E-02 |
| 7 | 1.737E-04 | 2.361E-01 | 2.363E-01 | 9.158E-05 | 6.196E-02 | 6.205E-02 | 9.548E-05 | 6.708E-02 | 6.717E-02 |
| 8 | -3.229E-06 | 1.053E-02 | 1.052E-02 | -8.547E-06 | 6.491E-03 | 6.482E-03 | -8.702E-06 | 6.885E-03 | 6.876E-03 |
| 9 | 0.0 | 0.0 | 0.0 | 8.967E-04 | 1.919E-02 | 2.009E-02 | 9.878E-04 | 2.055E-02 | 2.153E-02 |
| 10 | 0.0 | 0.0 | 0.0 | 3.302E-03 | -5.724E-03 | -2.422E-03 | 3.316E-03 | -5.149E-03 | -1.834E-03 |
| 11 | 0.0 | 0.0 | 0.0 | 2.757E-03 | 4.324E-02 | 4.600E-02 | 2.397E-03 | 4.059E-02 | 4.299E-02 |
| 12 | 0.0 | 0.0 | 0.0 | 6.906E-03 | -5.162E-03 | 1.744E-03 | 4.951E-03 | -3.874E-03 | 1.077E-03 |
| 13 | 0.0 | 0.0 | 0.0 | 3.930E-02 | -1.012E-03 | 3.828E-02 | 3.251E-02 | -6.989E-03 | 2.553E-02 |
| 14 | 0.0 | 0.0 | 0.0 | -1.112E-03 | -2.282E-04 | -1.340E-03 | -1.380E-03 | 1.290E-03 | -8.967E-05 |
| 15 | 0.0 | 0.0 | 0.0 | 2.145E-03 | -5.480E-04 | 1.597E-03 | 1.190E-01 | 2.642E-02 | 1.454E-01 |
| SUM | -8.842E-04 | 6.399E-01 | 6.390E-01 | 5.391E-02 | 1.994E-01 | 2.534E-01 | 1.615E-01 | 2.353E-01 | 3.967E-01 |

TABLE 34 - VIT.C-BABEL
BABEL Total effects

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|-----------|-----------|---------------|------------|------------|----------------|-----------|-----------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | 2.295E-05 | 2.837E-04 | 3.066E-04 | 7.243E-06 | 7.340E-05 | 8.064E-05 | 7.676E-06 | 7.879E-05 | 8.647E-05 |
| 2 | 5.887E-06 | 1.651E-03 | 1.657E-03 | 1.869E-06 | 4.206E-04 | 4.225E-04 | 1.980E-06 | 4.529E-04 | 4.540E-04 |
| 3 | 4.640E-06 | 1.675E-03 | 1.680E-03 | 1.307E-06 | 3.398E-04 | 3.411E-04 | 1.394E-06 | 3.707E-04 | 3.721E-04 |
| 4 | 2.783E-05 | 5.071E-03 | 5.099E-03 | 7.227E-06 | 9.557E-04 | 9.630E-04 | 7.727E-06 | 1.046E-03 | 1.054E-03 |
| 5 | 3.178E-05 | 4.140E-03 | 4.172E-03 | 1.098E-05 | 9.194E-04 | 9.304E-04 | 1.160E-05 | 9.994E-04 | 1.011E-03 |
| 6 | 6.753E-05 | 6.998E-03 | 7.065E-03 | 2.836E-05 | 1.712E-03 | 1.740E-03 | 2.973E-05 | 1.855E-03 | 1.885E-03 |
| 7 | 1.039E-04 | 7.199E-03 | 7.303E-03 | 5.353E-05 | 1.905E-03 | 1.958E-03 | 5.590E-05 | 2.060E-03 | 2.116E-03 |
| 8 | 1.018E-05 | 6.879E-04 | 6.981E-04 | 2.687E-05 | 4.759E-04 | 5.028E-04 | 2.736E-05 | 5.015E-04 | 5.288E-04 |
| 9 | 0.0 | 0.0 | 0.0 | 3.567E-04 | 1.311E-03 | 1.668E-03 | 3.729E-04 | 1.426E-03 | 1.799E-03 |
| 10 | 0.0 | 0.0 | 0.0 | 1.828E-04 | 6.434E-03 | 6.616E-03 | 1.655E-04 | 6.252E-03 | 6.418E-03 |
| 11 | 0.0 | 0.0 | 0.0 | 6.464E-05 | 3.720E-03 | 3.785E-03 | 5.620E-05 | 3.444E-03 | 3.500E-03 |
| 12 | 0.0 | 0.0 | 0.0 | 7.962E-04 | 3.294E-03 | 4.090E-03 | 6.532E-04 | 2.693E-03 | 3.346E-03 |
| 13 | 0.0 | 0.0 | 0.0 | 2.042E-02 | 2.367E-03 | 2.278E-02 | 1.705E-02 | 2.400E-03 | 1.945E-02 |
| 14 | 0.0 | 0.0 | 0.0 | 8.029E-04 | 2.957E-04 | 1.099E-03 | 5.568E-04 | 2.046E-04 | 7.014E-04 |
| 15 | 0.0 | 0.0 | 0.0 | 0.0 | -4.271E-06 | -4.271E-06 | 0.0 | 7.471E-06 | 7.471E-06 |
| SUM | 2.747E-04 | 2.771E-02 | 2.798E-02 | 2.276E-02 | 2.422E-02 | 4.696E-02 | 1.900E-02 | 2.379E-02 | 4.279E-02 |

TABLE 35 - PROPANE D₁-PROPANE D₀ Fe effects
PROPANE D₀

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| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|-----------|-----------|---------------|-----------|-----------|----------------|------------|-----------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | 1.849E-06 | 5.547E-04 | 5.566E-04 | 5.835E-07 | 1.444E-04 | 1.450E-04 | 6.184E-07 | 1.549E-04 | 1.555E-04 |
| 2 | 1.688E-07 | 2.256E-03 | 2.256E-03 | 5.361E-08 | 5.717E-04 | 5.718E-04 | 5.680E-08 | 6.146E-04 | 6.146E-04 |
| 3 | 3.261E-06 | 3.154E-02 | 3.155E-02 | 9.187E-07 | 6.777E-03 | 6.778E-03 | 9.793E-07 | 7.366E-03 | 7.367E-03 |
| 4 | 1.088E-05 | 1.862E-02 | 1.863E-02 | 2.826E-06 | 3.482E-03 | 3.485E-03 | 3.022E-06 | 3.808E-03 | 3.811E-03 |
| 5 | 6.002E-06 | 1.780E-02 | 1.781E-02 | 2.073E-06 | 3.922E-03 | 3.924E-03 | 2.190E-06 | 4.266E-03 | 4.268E-03 |
| 6 | 1.044E-05 | 5.221E-02 | 5.222E-02 | 4.386E-06 | 1.277E-02 | 1.277E-02 | 4.598E-06 | 1.383E-02 | 1.884E-02 |
| 7 | 2.177E-05 | 3.190E-02 | 3.192E-02 | 1.122E-05 | 8.225E-03 | 8.237E-03 | 1.172E-05 | 8.908E-03 | 8.920E-03 |
| 8 | 1.051E-06 | 2.286E-03 | 2.287E-03 | 2.772E-06 | 1.606E-03 | 1.609E-03 | 2.823E-06 | 1.692E-03 | 1.695E-03 |
| 9 | 0.0 | 0.0 | 0.0 | 1.231E-03 | 3.137E-02 | 3.260E-02 | 1.288E-03 | 3.414E-02 | 3.543E-02 |
| 10 | 0.0 | 0.0 | 0.0 | 1.326E-03 | 1.528E-03 | 2.855E-03 | 1.201E-03 | 1.469E-03 | 2.670E-03 |
| 11 | 0.0 | 0.0 | 0.0 | 3.338E-03 | 1.278E-03 | 4.616E-03 | 2.902E-03 | 1.189E-03 | 4.091E-03 |
| 12 | 0.0 | 0.0 | 0.0 | 8.793E-03 | 1.171E-03 | 9.965E-03 | 7.215E-03 | 9.667E-04 | 8.181E-03 |
| 13 | 0.0 | 0.0 | 0.0 | 1.588E-03 | 6.296E-04 | 2.217E-03 | 1.326E-03 | 6.340E-04 | 1.960E-03 |
| 14 | 0.0 | 0.0 | 0.0 | 2.232E-03 | 3.605E-04 | 2.593E-03 | 1.548E-03 | 2.508E-04 | 1.798E-03 |
| 15 | 0.0 | 0.0 | 0.0 | 6.714E-04 | 2.197E-05 | 6.933E-04 | 8.311E-04 | -3.855E-05 | 7.925E-04 |
| SUM | 5.543E-05 | 1.572E-01 | 1.572E-01 | 1.920E-02 | 7.385E-02 | 9.305E-02 | 1.634E-02 | 7.925E-02 | 9.559E-02 |

TABLE 36 - PROPANE DI-PROPANE D₀ Cr effects
PROPANE D₀

FAST FLUX 62 | TOTAL FLUX 62 | TOTAL FLUX 187

| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
|-------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| 1 | 2.214E-05 | 9.930E-05 | 1.219E-04 | 6.986E-06 | 2.622E-05 | 3.321E-05 | 7.403E-06 | 2.812E-05 | 3.552E-05 |
| 2 | 2.262E-05 | 4.060E-04 | 4.286E-04 | 7.182E-06 | 1.025E-04 | 1.097E-04 | 7.609E-06 | 1.103E-04 | 1.179E-04 |
| 3 | 1.317E-05 | 3.432E-03 | 3.445E-03 | 3.711E-06 | 7.450E-04 | 7.488E-04 | 3.956E-06 | 6.091E-04 | 8.131E-04 |
| 4 | 2.310E-05 | 3.039E-03 | 3.062E-03 | 6.000E-06 | 5.516E-04 | 5.576E-04 | 6.415E-06 | 6.043E-04 | 6.107E-04 |
| 5 | 1.043E-05 | 2.663E-03 | 2.673E-03 | 3.604E-06 | 5.967E-04 | 6.003E-04 | 3.808E-06 | 6.481E-04 | 6.519E-04 |
| 6 | 1.756E-05 | 2.807E-03 | 2.824E-03 | 7.374E-06 | 7.062E-04 | 7.136E-04 | 7.730E-06 | 7.632E-04 | 7.709E-04 |
| 7 | 2.814E-05 | 1.479E-02 | 1.482E-02 | 1.450E-05 | 3.790E-03 | 3.804E-03 | 1.514E-05 | 4.106E-03 | 4.121E-03 |
| 8 | 1.907E-06 | 4.140E-03 | 4.142E-03 | 5.032E-06 | 2.876E-03 | 2.881E-03 | 5.124E-06 | 3.030E-03 | 3.035E-03 |
| 9 | 0.0 | 0.0 | 0.0 | 6.228E-05 | 9.652E-02 | 9.659E-02 | 6.512E-05 | 1.055E-01 | 1.056E-01 |
| 10 | 0.0 | 0.0 | 0.0 | 3.359E-05 | 3.838E-03 | 3.871E-03 | 3.041E-05 | 3.710E-03 | 3.740E-03 |
| 11 | 0.0 | 0.0 | 0.0 | 4.854E-05 | 1.830E-02 | 1.835E-02 | 4.220E-05 | 1.722E-02 | 1.726E-02 |
| 12 | 0.0 | 0.0 | 0.0 | 2.479E-05 | 1.876E-03 | 1.901E-03 | 2.034E-05 | 1.543E-03 | 1.564E-03 |
| 13 | 0.0 | 0.0 | 0.0 | 4.912E-05 | 1.351E-03 | 1.400E-03 | 4.102E-05 | 1.361E-03 | 1.402E-03 |
| 14 | 0.0 | 0.0 | 0.0 | 2.708E-04 | 7.404E-04 | 1.011E-03 | 1.878E-04 | 5.102E-04 | 6.980E-04 |
| 15 | 0.0 | 0.0 | 0.0 | 7.498E-05 | 5.960E-05 | 1.346E-04 | 9.313E-05 | -1.051E-04 | -1.201E-05 |
| SUM | 1.391E-04 | 3.138E-02 | 3.152E-02 | 6.184E-04 | 1.321E-01 | 1.327E-01 | 5.372E-04 | 1.399E-01 | 1.404E-01 |

TABLE 37 - PROPANE D₁ - PROPANE D₀ Ni effects
PROPANE D₀

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 167 | | |
|-------|--------------|-----------|-----------|---------------|------------|-----------|----------------|-----------|-----------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | 1.440E-05 | 2.041E-04 | 2.185E-04 | 4.543E-06 | 5.278E-05 | 5.732E-05 | 4.815E-06 | 5.664E-05 | 6.145E-05 |
| 2 | 1.317E-07 | 1.131E-03 | 1.131E-03 | 4.180E-08 | 2.892E-04 | 2.892E-04 | 4.429E-08 | 3.107E-04 | 3.107E-04 |
| 3 | 1.439E-07 | 3.569E-03 | 3.570E-03 | 4.052E-08 | 7.400E-04 | 7.401E-04 | 4.319E-08 | 8.054E-04 | 8.054E-04 |
| 4 | 2.295E-08 | 2.425E-02 | 2.425E-02 | 5.960E-09 | 4.056E-03 | 4.056E-03 | 6.372E-09 | 4.481E-03 | 4.481E-03 |
| 5 | 1.233E-07 | 2.350E-02 | 2.350E-02 | 4.231E-08 | 5.107E-03 | 5.107E-03 | 4.472E-08 | 5.569E-03 | 5.569E-03 |
| 6 | 6.875E-07 | 1.627E-02 | 1.627E-02 | 2.814E-07 | 3.882E-03 | 3.882E-03 | 2.955E-07 | 4.228E-03 | 4.228E-03 |
| 7 | 2.942E-06 | 3.031E-02 | 3.031E-02 | 1.500E-06 | 7.690E-03 | 7.692E-03 | 1.567E-06 | 8.369E-03 | 8.371E-03 |
| 8 | 2.952E-07 | 2.906E-03 | 2.907E-03 | 5.585E-07 | 1.476E-03 | 1.476E-03 | 5.770E-07 | 1.580E-03 | 1.581E-03 |
| 9 | 0.0 | 0.0 | 0.0 | 3.743E-05 | 3.868E-02 | 3.872E-02 | 4.387E-05 | 4.641E-02 | 4.645E-02 |
| 10 | 0.0 | 0.0 | 0.0 | 1.353E-05 | 7.781E-03 | 7.795E-03 | 1.491E-05 | 1.326E-02 | 1.328E-02 |
| 11 | 0.0 | 0.0 | 0.0 | 1.211E-06 | 9.051E-03 | 9.052E-03 | 1.585E-06 | 1.706E-02 | 1.706E-02 |
| 12 | 0.0 | 0.0 | 0.0 | 1.001E-04 | 6.400E-03 | 6.500E-03 | 1.438E-04 | 9.314E-03 | 9.458E-03 |
| 13 | 0.0 | 0.0 | 0.0 | 8.581E-05 | 1.715E-03 | 1.801E-03 | 2.954E-04 | 6.595E-02 | 6.625E-02 |
| 14 | 0.0 | 0.0 | 0.0 | 3.897E-04 | 1.095E-03 | 1.485E-03 | 5.226E-03 | 1.326E-01 | 1.379E-01 |
| 15 | 0.0 | 0.0 | 0.0 | 3.636E-04 | -3.192E-05 | 3.317E-04 | 8.806E-03 | 1.452E-03 | 1.026E-02 |
| SUM | 1.875E-05 | 1.021E-01 | 1.022E-01 | 9.984E-04 | 8.799E-02 | 8.899E-02 | 1.454E-02 | 3.115E-01 | 3.260E-01 |

TABLE 38 - PROPANE D1-PROPANE D₀ Na effects
PROPANE D₀

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|-----------|-----------|---------------|-----------|-----------|----------------|-----------|-----------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | 6.134E-05 | 1.142E-03 | 1.204E-03 | 1.936E-05 | 2.968E-04 | 3.162E-04 | 2.051E-05 | 3.185E-04 | 3.390E-04 |
| 2 | 2.881E-05 | 5.444E-03 | 5.473E-03 | 9.147E-06 | 1.384E-03 | 1.393E-03 | 9.691E-06 | 1.488E-03 | 1.497E-03 |
| 3 | 2.121E-05 | 4.022E-02 | 4.024E-02 | 5.977E-06 | 8.602E-03 | 8.608E-03 | 6.372E-06 | 9.351E-03 | 9.358E-03 |
| 4 | 6.184E-05 | 5.098E-02 | 5.104E-02 | 1.606E-05 | 9.046E-03 | 9.062E-03 | 1.717E-05 | 9.939E-03 | 9.958E-03 |
| 5 | 4.834E-05 | 4.811E-02 | 4.816E-02 | 1.670E-05 | 1.054E-02 | 1.056E-02 | 1.764E-05 | 1.146E-02 | 1.150E-02 |
| 6 | 9.621E-05 | 7.828E-02 | 7.838E-02 | 4.040E-05 | 1.907E-02 | 1.911E-02 | 4.235E-05 | 2.068E-02 | 2.072E-02 |
| 7 | 1.567E-04 | 8.420E-02 | 8.435E-02 | 8.075E-05 | 2.161E-02 | 2.169E-02 | 8.432E-05 | 2.344E-02 | 2.353E-02 |
| 8 | 1.344E-05 | 1.002E-02 | 1.003E-02 | 3.523E-05 | 6.434E-03 | 6.469E-03 | 3.589E-05 | 6.803E-03 | 6.839E-03 |
| 9 | 0.0 | 0.0 | 0.0 | 1.688E-03 | 1.679E-01 | 1.696E-01 | 1.769E-03 | 1.875E-01 | 1.893E-01 |
| 10 | 0.0 | 0.0 | 0.0 | 1.556E-03 | 1.958E-02 | 2.114E-02 | 1.412E-03 | 2.469E-02 | 2.611E-02 |
| 11 | 0.0 | 0.0 | 0.0 | 3.452E-03 | 3.235E-02 | 3.580E-02 | 3.002E-03 | 3.891E-02 | 4.191E-02 |
| 12 | 0.0 | 0.0 | 0.0 | 9.715E-03 | 1.274E-02 | 2.246E-02 | 8.032E-03 | 1.452E-02 | 2.255E-02 |
| 13 | 0.0 | 0.0 | 0.0 | 2.214E-02 | 6.063E-03 | 2.820E-02 | 1.871E-02 | 7.035E-02 | 8.906E-02 |
| 14 | 0.0 | 0.0 | 0.0 | 3.695E-03 | 2.492E-03 | 6.187E-03 | 7.518E-03 | 1.336E-01 | 1.411E-01 |
| 15 | 0.0 | 0.0 | 0.0 | 1.110E-03 | 4.538E-05 | 1.155E-03 | 9.730E-03 | 1.316E-03 | 1.105E-02 |
| SUM | 4.879E-04 | 3.184E-01 | 3.189E-01 | 4.358E-02 | 3.181E-01 | 3.617E-01 | 5.041E-02 | 5.544E-01 | 6.048E-01 |

TABLE 39 - PROPANE D1-PROPANE D₀ Total effects
PROPANE D₀

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| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -1.085E-05 | 1.470E-05 | 3.853E-06 | 3.424E-06 | 3.804E-06 | 3.799E-07 | -3.629E-06 | 4.084E-06 | 4.551E-07 |
| 2 | -3.975E-05 | -2.963E-06 | -4.271E-05 | -1.262E-05 | -7.550E-07 | -1.338E-05 | -1.337E-05 | -8.114E-07 | -1.418E-05 |
| 3 | -1.005E-04 | -2.137E-03 | -2.237E-03 | -2.830E-05 | -4.335E-04 | -4.618E-04 | -3.017E-05 | -4.728E-04 | -5.030E-04 |
| 4 | -4.147E-03 | -9.207E-03 | -1.335E-02 | -1.077E-03 | -1.735E-03 | -2.812E-03 | -1.151E-03 | -1.899E-03 | -3.050E-03 |
| 5 | -2.329E-03 | -4.953E-04 | -2.824E-03 | -8.044E-04 | -1.100E-04 | -9.144E-04 | -8.500E-04 | -1.196E-04 | -9.695E-04 |
| 6 | 7.860E-04 | -4.477E-03 | -3.691E-03 | 3.301E-04 | -1.095E-03 | -7.652E-04 | 3.460E-04 | -1.187E-03 | -8.406E-04 |
| 7 | 4.236E-03 | -8.208E-03 | -3.973E-03 | 2.183E-03 | -2.172E-03 | 1.108E-05 | 2.279E-03 | -2.349E-03 | -6.909E-05 |
| 8 | 1.829E-04 | 1.485E-02 | 1.503E-02 | 4.825E-04 | 1.027E-02 | 1.076E-02 | 4.913E-04 | 1.083E-02 | 1.132E-02 |
| 9 | 0.0 | 0.0 | 0.0 | 7.789E-03 | 5.350E-02 | 6.129E-02 | 8.143E-03 | 5.821E-02 | 6.635E-02 |
| 10 | 0.0 | 0.0 | 0.0 | 1.524E-03 | 7.102E-04 | 2.235E-03 | 1.380E-03 | 6.902E-04 | 2.070E-03 |
| 11 | 0.0 | 0.0 | 0.0 | -1.819E-03 | -2.242E-03 | -4.062E-03 | -1.582E-03 | -2.076E-03 | -3.657E-03 |
| 12 | 0.0 | 0.0 | 0.0 | 5.410E-03 | 1.006E-03 | 6.416E-03 | 4.439E-03 | 8.222E-04 | 5.261E-03 |
| 13 | 0.0 | 0.0 | 0.0 | 2.800E-02 | 3.777E-03 | 3.178E-02 | 2.338E-02 | 3.829E-03 | 2.721E-02 |
| 14 | 0.0 | 0.0 | 0.0 | 6.563E-03 | 9.318E-04 | 7.495E-03 | 4.551E-03 | 6.447E-04 | 5.196E-03 |
| 15 | 0.0 | 0.0 | 0.0 | -2.232E-04 | -4.268E-05 | -2.658E-04 | -2.767E-04 | 7.466E-05 | -2.021E-04 |
| SUM | -1.423E-03 | -9.662E-03 | -1.108E-02 | 4.831E-02 | 6.237E-02 | 1.107E-01 | 4.110E-02 | 6.699E-02 | 1.081E-01 |

TABLE 40 - VIT.E-VIT.C Fe effects
VIT.C

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -3.626E-04 | 1.670E-04 | -1.955E-04 | +1.144E-04 | 4.349E-05 | -7.093E-05 | -1.213E-04 | 4.665E-05 | -7.461E-05 |
| 2 | -2.206E-04 | 8.926E-05 | -1.314E-04 | +7.006E-05 | 2.262E-05 | -4.743E-05 | -7.422E-05 | 2.432E-05 | -4.990E-05 |
| 3 | -5.197E-05 | -4.785E-04 | -5.305E-04 | -1.464E-05 | -1.028E-04 | -1.175E-04 | -1.561E-05 | -1.117E-04 | -1.274E-04 |
| 4 | -1.461E-02 | -1.043E-04 | -1.471E-02 | -3.793E-03 | -1.951E-05 | -3.812E-03 | -4.055E-03 | -2.134E-05 | -4.077E-03 |
| 5 | -2.722E-03 | 3.600E-02 | 3.328E-02 | -9.402E-04 | 7.932E-03 | 6.991E-03 | -9.934E-04 | 8.628E-03 | 7.635E-03 |
| 6 | 8.224E-06 | -5.730E-04 | -5.647E-04 | 3.454E-06 | -1.401E-04 | -1.366E-04 | 3.621E-06 | -1.518E-04 | -1.482E-04 |
| 7 | 7.342E-06 | 3.964E-04 | 4.037E-04 | 3.784E-06 | 1.022E-04 | 1.060E-04 | 3.951E-06 | 1.107E-04 | 1.147E-04 |
| 8 | 1.083E-06 | 6.863E-05 | 6.972E-05 | 2.858E-06 | 4.822E-05 | 5.108E-05 | 2.911E-06 | 5.079E-05 | 5.370E-05 |
| 9 | 0.0 | 0.0 | 0.0 | 3.615E-04 | 2.220E-03 | 2.582E-03 | 3.780E-04 | 2.617E-03 | 2.795E-03 |
| 10 | 0.0 | 0.0 | 0.0 | 4.045E-05 | -8.493E-04 | -8.089E-04 | 3.662E-05 | -8.162E-04 | -7.796E-04 |
| 11 | 0.0 | 0.0 | 0.0 | 4.120E-06 | 3.943E-05 | 4.355E-05 | 3.582E-06 | 3.668E-05 | 4.026E-05 |
| 12 | 0.0 | 0.0 | 0.0 | 1.283E-03 | 9.000E-05 | 1.373E-03 | 1.052E-03 | 7.428E-05 | 1.127E-03 |
| 13 | 0.0 | 0.0 | 0.0 | 6.672E-05 | 3.101E-04 | 3.768E-04 | 5.572E-05 | 3.122E-04 | 3.679E-04 |
| 14 | 0.0 | 0.0 | 0.0 | -9.507E-05 | 5.930E-05 | -3.577E-05 | -6.592E-05 | 4.126E-05 | -2.466E-05 |
| 15 | 0.0 | 0.0 | 0.0 | -2.046E-04 | -9.816E-06 | -2.144E-04 | -2.533E-04 | 1.723E-05 | -2.361E-04 |
| SUM | -1.795E-02 | 3.557E-02 | 1.762E-02 | -3.466E-03 | 9.746E-03 | 6.279E-03 | -4.042E-03 | 1.066E-02 | 6.616E-03 |

TABLE 41. - VIT.E-VIT.C Cr effects
VIT.C

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| GROUP | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | 5.006E-05 | -1.588E-04 | -1.087E-04 | 1.580E-05 | -4.172E-05 | -2.592E-05 | 1.674E-05 | -4.474E-05 | -2.799E-05 |
| 2 | -7.400E-05 | -7.800E-04 | -8.540E-04 | -2.350E-05 | -1.970E-04 | -2.205E-04 | -2.490E-05 | -2.119E-04 | -2.368E-04 |
| 3 | 4.199E-04 | -5.150E-03 | -4.730E-03 | 1.183E-04 | -1.118E-03 | -9.998E-04 | 1.261E-04 | -1.214E-03 | -1.088E-03 |
| 4 | 4.015E-05 | -1.643E-02 | -1.639E-02 | 1.043E-05 | -2.983E-03 | -2.972E-03 | 1.115E-05 | -3.267E-03 | -3.256E-03 |
| 5 | -5.095E-05 | -9.086E-04 | -9.595E-04 | -1.760E-05 | -2.036E-04 | -2.212E-04 | -1.859E-05 | -2.211E-04 | -2.397E-04 |
| 6 | 5.819E-06 | 2.199E-04 | 2.257E-04 | 2.444E-06 | 5.534E-05 | 5.778E-05 | 2.562E-06 | 5.981E-05 | 6.237E-05 |
| 7 | 9.852E-06 | -6.020E-04 | -5.921E-04 | 5.077E-06 | -1.542E-04 | -1.491E-04 | 5.302E-06 | -1.671E-04 | -1.618E-04 |
| 8 | 1.598E-06 | 3.713E-04 | 3.729E-04 | 4.217E-06 | 2.579E-04 | 2.621E-04 | 4.295E-06 | 2.717E-04 | 2.760E-04 |
| 9 | 0.0 | 0.0 | 0.0 | 1.836E-04 | 3.409E-03 | 3.593E-03 | 1.920E-04 | 3.727E-03 | 3.919E-03 |
| 10 | 0.0 | 0.0 | 0.0 | 4.582E-05 | 2.197E-04 | 2.655E-04 | 4.148E-05 | 2.124E-04 | 2.539E-04 |
| 11 | 0.0 | 0.0 | 0.0 | 5.847E-05 | 9.891E-04 | 1.048E-03 | 5.084E-05 | 9.305E-04 | 9.813E-04 |
| 12 | 0.0 | 0.0 | 0.0 | 1.478E-04 | -4.272E-05 | 1.051E-04 | 1.212E-04 | -3.515E-05 | 8.609E-05 |
| 13 | 0.0 | 0.0 | 0.0 | -1.052E-06 | 3.004E-04 | 2.993E-04 | -8.786E-07 | 3.024E-04 | 3.016E-04 |
| 14 | 0.0 | 0.0 | 0.0 | 1.060E-04 | 5.183E-05 | 1.578E-04 | 7.351E-05 | 3.572E-05 | 1.092E-04 |
| 15 | 0.0 | 0.0 | 0.0 | -1.091E-04 | -2.137E-05 | -1.305E-04 | -1.355E-04 | 3.769E-05 | -9.784E-05 |
| SUM | 4.025E-04 | -2.344E-02 | -2.304E-02 | 5.467E-04 | 5.220E-04 | 1.069E-03 | 4.653E-04 | 4.157E-04 | 8.811E-04 |

TABLE 42 - VIT.E-VIT.C Ni effects
VIT.C

| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -1.097E-06 | -7.684E-04 | -7.695E-04 | 3.456E-07 | -1.987E-04 | -1.990E-04 | -3.664E-07 | -2.132E-04 | -2.136E-04 |
| 2 | 2.360E-08 | -3.062E-03 | -3.062E-03 | 7.497E-09 | -7.829E-04 | -7.829E-04 | 7.942E-09 | -8.411E-04 | -8.411E-04 |
| 3 | 1.184E-07 | -8.150E-03 | -8.150E-03 | 3.339E-08 | -1.691E-03 | -1.691E-03 | 3.559E-08 | -1.840E-03 | -1.840E-03 |
| 4 | 1.338E-06 | -4.641E-02 | -4.641E-02 | 3.422E-07 | -7.781E-03 | -7.781E-03 | 3.662E-07 | -8.598E-03 | -8.597E-03 |
| 5 | 5.584E-07 | -3.566E-02 | -3.566E-02 | 1.861E-07 | -7.772E-03 | -7.772E-03 | 1.969E-07 | -8.479E-03 | -8.479E-03 |
| 6 | -4.139E-05 | -1.601E-02 | -1.605E-02 | -1.573E-05 | -3.852E-03 | -3.868E-03 | -1.661E-05 | -4.206E-03 | -4.222E-03 |
| 7 | 8.577E-05 | -4.279E-02 | -4.271E-02 | 3.225E-05 | -1.091E-02 | -1.087E-02 | 3.457E-05 | -1.197E-02 | -1.194E-02 |
| 8 | 7.011E-06 | 1.074E-02 | 1.075E-02 | -1.778E-05 | 3.071E-03 | 3.054E-03 | -1.674E-05 | 3.479E-03 | 3.463E-03 |
| 9 | 0.0 | 0.0 | 0.0 | 1.073E-03 | -3.201E-03 | -2.128E-03 | 1.285E-03 | -4.539E-03 | -3.255E-03 |
| 10 | 0.0 | 0.0 | 0.0 | 6.125E-04 | -2.539E-03 | -1.927E-03 | 8.163E-04 | -8.511E-03 | -7.695E-03 |
| 11 | 0.0 | 0.0 | 0.0 | 1.921E-04 | -5.020E-03 | -4.828E-03 | 2.950E-04 | -1.279E-02 | -1.249E-02 |
| 12 | 0.0 | 0.0 | 0.0 | 2.948E-03 | 6.588E-03 | 9.537E-03 | 4.135E-03 | 7.875E-03 | 1.201E-02 |
| 13 | 0.0 | 0.0 | 0.0 | 4.520E-03 | 7.547E-05 | 4.596E-03 | 1.933E-02 | -1.674E-03 | 1.765E-02 |
| 14 | 0.0 | 0.0 | 0.0 | 1.015E-03 | -4.437E-05 | 9.707E-04 | 9.062E-03 | -3.391E-03 | 5.671E-03 |
| 15 | 0.0 | 0.0 | 0.0 | -2.567E-03 | 7.367E-05 | -2.493E-03 | -6.275E-02 | -3.740E-03 | -6.649E-02 |
| SUM | 5.233E-05 | -1.421E-01 | -1.421E-01 | 7.794E-03 | -3.398E-02 | -2.618E-02 | -2.783E-02 | -5.944E-02 | -8.727E-02 |

TABLE 43 - VIT.E-VIT.C
Na effects
VIT.C

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| | FAST FLUX 62 | | | TOTAL FLUX 62 | | | TOTAL FLUX 187 | | |
|-------|--------------|------------|------------|---------------|------------|------------|----------------|------------|------------|
| GROUP | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL | ABSORPT. | SCATTER. | TOTAL |
| 1 | -3.245E-04 | -7.454E-04 | -1.070E-03 | -1.024E-04 | -1.931E-04 | -2.955E-04 | -1.085E-04 | -2.072E-04 | -3.157E-04 |
| 2 | -3.344E-04 | -3.756E-03 | -4.090E-03 | -1.062E-04 | -9.580E-04 | -1.064E-03 | -1.125E-04 | -1.029E-03 | -1.142E-03 |
| 3 | 2.676E-04 | -1.592E-02 | -1.565E-02 | 7.541E-05 | -3.345E-03 | -3.270E-03 | 8.038E-05 | -3.639E-03 | -3.559E-03 |
| 4 | -1.871E-02 | -7.215E-02 | -9.086E-02 | -4.859E-03 | -1.252E-02 | -1.738E-02 | -5.195E-03 | -1.379E-02 | -1.898E-02 |
| 5 | -5.101E-03 | -1.062E-03 | -6.164E-03 | -1.762E-03 | -1.540E-04 | -1.916E-03 | -1.862E-03 | -1.919E-04 | -2.054E-03 |
| 6 | 7.586E-04 | -2.084E-02 | -2.008E-02 | 3.203E-04 | -5.032E-03 | -4.712E-03 | 3.356E-04 | -5.484E-03 | -5.149E-03 |
| 7 | 4.339E-03 | -5.121E-02 | -4.687E-02 | 2.224E-03 | -1.313E-02 | -1.091E-02 | 2.323E-03 | -1.437E-02 | -1.205E-02 |
| 8 | 1.925E-04 | 2.603E-02 | 2.623E-02 | 4.718E-04 | 1.365E-02 | 1.412E-02 | 4.818E-04 | 1.463E-02 | 1.511E-02 |
| 9 | 0.0 | 0.0 | 0.0 | 9.407E-03 | 5.593E-02 | 6.533E-02 | 9.998E-03 | 5.981E-02 | 6.981E-02 |
| 10 | 0.0 | 0.0 | 0.0 | 2.223E-03 | -2.458E-03 | -2.352E-04 | 2.274E-03 | -8.425E-03 | -6.150E-03 |
| 11 | 0.0 | 0.0 | 0.0 | -1.565E-03 | -6.234E-03 | -7.798E-03 | -1.232E-03 | -1.390E-02 | -1.513E-02 |
| 12 | 0.0 | 0.0 | 0.0 | 9.789E-03 | 7.641E-03 | 1.743E-02 | 9.747E-03 | 8.736E-03 | 1.848E-02 |
| 13 | 0.0 | 0.0 | 0.0 | 3.258E-02 | 4.463E-03 | 3.705E-02 | 4.276E-02 | 2.769E-03 | 4.553E-02 |
| 14 | 0.0 | 0.0 | 0.0 | 7.589E-03 | 9.986E-04 | 8.588E-03 | 1.362E-02 | -2.670E-03 | 1.095E-02 |
| 15 | 0.0 | 0.0 | 0.0 | -3.103E-03 | -1.926E-07 | -3.104E-03 | -6.342E-02 | -3.611E-03 | -6.703E-02 |
| SUM | -1.891E-02 | -1.396E-01 | -1.586E-01 | 5.319E-02 | 3.866E-02 | 9.185E-02 | 9.695E-03 | 1.863E-02 | 2.832E-02 |

TABLE 44 - VIT.E-VIT.C Total effects
VIT.C

PART II

1 - Introduction

The following analysis of some of the major results of the LMFBR benchmark exercise was made using the fifteen-group cross section sets provided by the participants. These cross sections are explicitly given in some of the tables in Part I of the present document. For the sake of simplicity, some of the data already provided in Part I are duplicated in some tables of Part II.

The benchmark specifications, the responses requested and the fifteen energy group structure can be found in Annex I of the present document.

2 - GENERAL FEATURES OF THE NEUTRON DATA LIBRARIES

The benchmark solutions obtained up to now are largely based on ENDF/B data :

- VITAMIN - E (ORNL) on ENDF/B version 5
- VITAMIN - C (ORNL) ; JSD-100 file data (RADHEAT - Japan), EURLIB, BABEL & PROPANE-D₀ data (CEA/CNEN solutions) are based on ENDF/B version 4.

On the contrary, the PROPANE - D₁ data are adjusted data based on neutron propagation experiments. Moreover, UKNDL data were used (UKAEA data).

Three main types of data processing methods have been used :

- 1 - $1/\Sigma_t$ type of weighting to process cross sections from the point data to multigroup data (VITAMIN - C and E, RADHEAT data /2,3,4/).
- 2 - Ultrafine flux weighting, mixture dependent, to take into account several self-shielding effects (BABEL data) /5/.

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3 - Starting from data of method 2, a successive space dependent shielding procedure can be used to further reduce the number of energy groups. This procedure was applied to produce the PROPANE D₀ formulaire data /6/.

The PROPANE D1 data are based on the PROPANE D₀ formulaire, but are adjusted on neutron propagation experiments in sodium/steel mixtures, in the framework of the CEA/CNEN Cooperation /7,8/.

The UK data, supplied by McCracken and Miller, included also continuous Monte Carlo calculations, based on UKNDL data, using the Monte Carlo DUCKPOND code.

3 - MAIN RESULT DESCRIPTION

The main results are shown in tables 1 - 3.

3.1 TOTAL FLUX AND THE SODIUM CAPTURE RATE (Table 1)

Responses

The total flux and the sodium capture rate result dispersions are fairly large, in particular for the Na (n,γ) capture rate (sometime, more than a factor of two). In fact, one would expect a lower dispersion in view of the common origin of many data sets.

In fact, two groups of solutions seem to be present, namely the group of solutions based on the $1/\Sigma_t$ - type of processing, and the group based on ultrafine group flux weighting, which give consistently lower flux values.

In particular, lower flux values (~ 30 ÷ 40 %) are observed in the lateral shield, and the discrepancy stays more or less constant in the sodium tank up to the heat exchanger (mesh 187). This seems to indicate that a possible role is played by the stainless-steel cross section processing. Pure sodium cross section are presumably less affected by the processing procedure ($1/\Sigma_t$ or ultrafine flux weighting for a pure sodium mixture, being very close).

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In fact the additional discrepancy between BABEL and VITAMIN - C on Φ_{tot} in the sodium tank (i.e. between mesh 62 and 187) is $\sim 15\%$, i.e. of the same order of magnitude found between two $1/\Sigma_t$ - weighted data sets (RADHEAT and VITAMIN - C data at mesh interval 187). It is worth noting that the adjusted data tend to increase substantially the calculated unadjusted results.

3.2 HIGH ENERGY RESPONSES (TAB. 2)

The high energy responses ($\Phi > 100$ KeV and the stainless-steel damage response, DPA) show also large dispersions. In particular, as it could have been expected, the high energy flux at deep penetration is strongly affected by both data and processing method differences. Differences on the DPA response is somewhat lower, due to the low energy neutron contribution at deep penetration.

Moreover it should be noted that some inconsistency can exist in the data presented, since both iron and steel DPA data are sometime quoted.

3.3 γ - HEATING AND n - HEATING DATA (TAB. 3)

The γ - heating data are fairly consistent, in particular if data up to mesh 62 are considered and which are shown in table 3. The neutron heating data are also consistent, except for the RADHEAT data at mesh 62.

In summary both method and data influence the comparison among the different solutions. In section 4 some results of sensitivity analysis will be used to point out major data uncertainty effects and in section 6 some method related effects will be examined.

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4 - SENSITIVITY ANALYSIS

Sensitivity coefficients were requested for both the original group structure (i.e. consistent with the multigroup data used) and for the reduced 15 energy group structure. A remarkable agreement is found in both the shape and the numerical values of the sensitivity profiles, which were calculated basically from two different code systems, the SWANLAKE /9/ system, and the SAMPO System /10/.

In Part I of the present paper, some sensitivity coefficients are provided in tables 4-3 for the different isotopes (Fe, Cr, Ni and Na, both in the lateral shield and in the Na tank). These are region integrated values relative to the fast flux at mesh 62 and to the total flux at meshes 62 and 187.

The folding of these sensitivity coefficients and of the 15 energy group cross section data supplied by the participants gives an indicative explanation of the discrepancies observed in tables 1 - 3. For example, some results of this exercise are shown in tables 20 and 24, where the VITAMIN - E/BABEL discrepancies are shown group-wise for the fast flux and the total flux.

The total effects (table 10) are fairly representative of the exact discrepancy data of table 1 and 2, even if some non-linear effects and group structure dependent effects are also present :

| DISCREPANCY BETWEEN VITAMIN - E AND BABEL | | |
|---|-------------------------|--------------------------|
| | Based on direct calcul. | Based on sens 15 g calc. |
| Fast flux at mesh 62 | 107 % | 48 % |
| Total flux at mesh 62 | 58 % | 34 % |
| Total flux at mesh 187 | 73 % | 42 % |

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The results for the total flux response of the tables show the predominant role played by the iron data (table 20) in particular the scattering data below ~ 300 KeV and the capture data in the region below ~ 2 KeV. Self-shielding effects could be at the origin of some of the observed discrepancies.

In the case of the fast flux response, the iron data indicate a strong effect of the scattering data below 1.35 MeV. Since Fe inelastic cross sections are different from zero only in the first four groups of the 15 energy group structure, these effects are mainly due to elastic scattering. Discrepancies of the order of 10 % in the scattering cross sections produce the observed fast flux response discrepancy.

5 - UNCERTAINTY ANALYSIS

To compare the observed discrepancies with the expected discrepancies on the basis of data uncertainty assessments, it was requested to the participants to fold the sensitivity coefficients with evaluated error matrices. The ORNL results indicate the following values, based on the existing ENDF/B - V uncertainty files, and on the ENDF/B - IV based 15 group covariances of Drischler and Weisbin /11/ :

| Uncertainty on : | ENDF/B - V | | ENDF/B - IV | |
|----------------------------------|----------------------|-------------|----------------------|-------------|
| | Uncertainty Value | Correlation | Uncertainty Value | Correlation |
| Fe damage at mesh 20 | 4 % | { 25 % | 3.4 % | { 31 % |
| Sodium Activation at mesh 187 | 65 % | | 69 % | |

No other participant has supplied a consistent estimate of data uncertainty effects. However several hypothesis can be made on data uncertainties and indicative results can be obtained on the uncertainty of the different responses. For example the following data are obtained in the case of the total flux at mesh 187 :

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| UNCERTAINTY ON σ_a AND σ_s | CORRELATION IN ENERGY | EFFECT ON TOTAL FLUX AT MESH 187 |
|---|-----------------------|----------------------------------|
| σ_a : 1 % σ_s : 10 % | 1.0 | 105 % |
| | 0.5 | 84 % |
| | 0. | 56 % |
| σ_a : 10 % σ_s : 10 % | 1.0 | 108 % |
| | 0.5 | 88 % |
| | 0. | 60 % |
| σ_a : 50 % σ_s : 10 % | 1.0 | 171 % |
| | 0.5 | 150 % |
| | 0. | 125 % |
| σ_a : 50 % σ_s : 20 % | 1.0 | 250 % |
| | 0.5 | 209 % |
| | 0. | 158 % |

The results obtained show the predominant role played by σ_s uncertainties and that only very large uncertainties on σ_a can be relevant in the global uncertainty assessment. Finally, the impact of correlations is certainly very important, as it has been often stressed, even in the simplified calculations of the previous table.

6 - METHOD EFFECTS

The main solutions allowed also to analyse the impact of the method approximations on the benchmark calculated results. The proposed reference solution had a fixed mesh size grid (approximately 3 cm in steel/sodium mixtures and 4 cm in sodium), S_N order $N = 4$ and P_1 Legendre polynomial expansion order.

The participants provided data obtained in S_{16} , P_3 and with a doubled space mesh grid.

The results are summarized in tables 45 and 46. The following commentaries can be made :

- There is excellent agreements between VITAMIN - E and BABEL calculated effects. Similar effects, but somewhat different in absolute value, are shown by RADHEAT calculations.
- Method effects systematically give higher calculated values with respect to the simplified reference model ($\sim 20\%$ for ϕ_{tot} and ϕ_{theq} on the HE).
- High energy flux is strongly affected, as it could be expected, by method effects.
- Separate effect analysis, show comparable order of magnitude of the different effects with a slight increase of S_N effects with propagation, except for P_n and, more pronounced, space mesh size in the case of the $\phi > 100$ KeV response (up to a factor of 4 global underestimation at mesh 187).

In conclusion, method approximations seems to be sufficiently understood. Major problems are certainly related to the correct modeling of 3D geometrical effects.

Finally, some processing effects have been investigated. In particular in table 47 we have indicated the effect on some typical response functions of the type of weighting used to generate multigroup cross section.

The influence of the fine weighting spectrum is large and the use of an appropriate method to handle self-shielding seems to be mandatory.

In this respect, the Monte Carlo results provided by UK and shown in table 48 seem to indicate that large discrepancies can be found if two widely different processing strategies are used. This indication applies to low energy responses, the high energy responses being in fairly good agreement. Therefore, if no normalization problem exists between the ANISN and DUCKPOND calculations, the results seem to indicate a larger self-shielding of resonances in the Monte Carlo calculations. Several participants at the meeting expressed their intention to perform more comparisons of that type.

Concerning the processing of scattering data, we have compared in the 15 group structure, the results obtained by two different, widely used codes to generate multigroup data, SUPERTOG and MC² - 2. Table 42 presents the results obtained for Fe. The inelastic scattering data compare fairly well, with the exception of the data close to the inelastic threshold. No major effect was found in the detailed inelastic matrix comparison.

In the case of elastic scattering, we have compared both the elastic $\sigma_{j \rightarrow j}$ and $\sigma_{j \rightarrow j+1}$ data for Fe. The infinite dilution data show the effect of the different algorithms of the two codes. The $\sigma_{j \rightarrow j}$ are in general good agreement with the exception of group 9 (273 - 67.4 KeV) where a discrepancy of ~ 8 % is observed. Larger discrepancies are found in the elastic removal data, $\sigma_{j \rightarrow j+1}$, where, in the intermediate range, 10 ÷ 20 % differences are often found.

Even if it is difficult to draw general conclusions from the data presented, there is evidence of the well known difficulty of assessing the uncertainty associated to the data processing codes, both from the point of view of comparing different multigroup processing codes /12/, and from the point of view of comparing different data processing strategies /13/.

7 - CONCLUSIONS

At the present stage, more data should be compared and a more deep insight in many of the observed results is necessary. This will be the main objective of the coming specialist meeting.

However, the present picture indicates a somewhat improved situation in data dispersion, with respect to the previous Vienna 1976 meeting.

Since the data analysed so far are in general related to the ENDF/B files, the main discrepancies observed are due a) to data processing methods and b) to the effects of data adjustments on the basis of integral experiments. The method approximations seem to be well understood, even if they are difficult to extrapolate to more complex geometries.

The use of the sensitivity analysis, now a very well established technique, will help in identifying areas of uncertainties and needs for improvements.

Finally, the subject of target accuracies has not been explicitly touched in the benchmark exercise. It will be of interest to evaluate the possible impact of the discrepancies observed in the benchmark exercise on the assessment both of the present state of data uncertainties and on the design target accuracies.

It seems in fact that uncertainties other than data uncertainties should be taken into account in a global uncertainty assessment. In this perspective, the notion of design target accuracy could possibly evolve to take into account the need for defining appropriate bias factors on the major quantities of interest.

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8 - REFERENCES

1 - M. SALVATORES

"Definition of a Fast Breeder Reactor Benchmark Configuration for Comparison of Shielding Cross Section Data", distributed by the NEA Data Bank, 16/03/1981.

2 - R.W. ROUSSIN et al.

ORNL - RSIC - 37 (1978).

3 - C.R. WEISBIN et al.

ORNL - TM - 5505 (1979).

4 - N. OHTANI

Contribution to the NEACRP benchmark

, 5 - J.C. ESTIOT et al.

Proc. Conf. on Neutron Physics and Neutron Data
HARWELL (1978).

6 - J.P. TRAPP et al.

Knoxville Conference on Nuclear Data and Technology (1979)

7 - J.P. TRAPP

OECD Specialists' Meeting on Nuclear data and Benchmarks for Shielding, Paris 1980.

8 - A. DE CARLI et al.

Ibidem

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9 - D.E. BARTINE et al.

The SWANLAKE System, ORNL - TM - 3809 (1973).

10 - G. PALMIOTTI et al

The SAMPO System

OECD Specialists' Meeting on Nuclear Data and Benchmarks for
Shielding, Paris 1980.

11 - J. DRISCHLER and C. WEISBIN,

ORNL Report

12 - C. WEISBIN et al.

ANS Atlanta Conference 1974

13 - M. GOLDSTEIN

ANS Sun Valley Conference 1980

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| | Φ_{total} | | | | $\Phi_{\text{th eq}}$ | | | |
|-------------|-----------------------|-------|-------|-------|-----------------------|-------|-------|-------|
| | 20 | 62 | 124 | 187 | 20 | 62 | 124 | 187 |
| VITAMIN - E | 1.008 | 1.103 | 1.149 | 1.214 | 1.009 | 1.100 | 1.137 | 1.189 |
| RADHEAT | 1.010 | 1.073 | 1.104 | 1.154 | 1.996 | 1.041 | 1.044 | 1.047 |
| BABEL | 1.0 | 1.122 | 1.148 | 1.209 | 1.0 | 1.089 | 1.140 | 1.202 |

| | $\Phi > 100 \text{ KeV}$ | | | | DPA | | $^{58}\text{Co}(n,\gamma)$ | |
|-------------|--------------------------|-------|-------|------|-------|-------|----------------------------|-------|
| | 20 | 62 | 124 | 187 | 20 | 62 | 20 | 62 |
| VITAMIN - E | 1.012 | 1.212 | 1.711 | 3.81 | 1.010 | 1.152 | 1.007 | 1.098 |
| RADHEAT | 1.011 | 1.189 | 1.61 | 4.23 | 1. | 1.083 | 1. | 1.112 |
| BABEL | 1.008 | 1.204 | 1.741 | 3.87 | 1.010 | 1.140 | 1. | 1.100 |

TABLE 45
GLOBAL METHOD APPROXIMATION EFFECTS

($S_4 P_1 \Delta x \rightarrow S_{16} P_3 (\Delta x/2)$)

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| | Φ_{total} | | | $\Phi_{\text{th eq}}$ | | |
|-----------------------------------|-----------------------|-------|-------|-----------------------|-------|-------|
| | 62 | 124 | 187 | 62 | 124 | 187 |
| $P_1 \rightarrow P_3$ | 1.028 | 1.039 | 1.052 | 1.019 | 1.034 | 1.046 |
| $S_4 \rightarrow S_{16}$ | 1.035 | 1.048 | 1.091 | 0.965 | 1.040 | 1.132 |
| $\Delta x \rightarrow \Delta x/2$ | 1.036 | 1.054 | 1.058 | 1.117 | 1.057 | 1.003 |

| | $\phi > 100 \text{ KeV}$ | | | DPA | $\text{Co } (n, \gamma)$ |
|-----------------------------------|--------------------------|-------|------|-------|--------------------------|
| | 62 | 124 | 187 | 62 | 62 |
| $P_1 \rightarrow P_3$ | 1.098 | 1.27 | 1.41 | 1.06 | 1.025 |
| $S_4 \rightarrow S_{16}$ | 1.099 | 1.087 | 1.05 | 1.082 | 1.021 |
| $\Delta x \rightarrow \Delta x/2$ | 1.004 | 1.237 | 2.57 | 1.003 | 1.049 |

TABLE 46
SEPARATE METHOD APPROXIMATION EFFECTS

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| | Φ_{total} | | $\Phi_{\text{th eq}}$ | | $\Phi > 820\text{KeV}$ | $\Phi > 14\text{KeV}$ |
|--------|-----------------------|------|-----------------------|------|------------------------|-----------------------|
| | 62 | 187 | 62 | 187 | 62 | 62 |
| Case 1 | 1.84 | 2.04 | 1.67 | 1.98 | 1.20 | 2.04 |
| Case 2 | 1.17 | 1.22 | 1.15 | 1.22 | 1.07 | 1.25 |
| Case 3 | 1.22 | 1.26 | 1.19 | 1.26 | 1.06 | 1.28 |

Reference case : Fe, Cr, Ni and Na weighted in a 50/50 SS/Na mixture spectrum

Case 1 : Fe weighted in a 100 % Fe spectrum. The other isotopes as reference

Case 2 : Fe weighted in a 100 % SS spectrum. The other isotopes as reference

Case 3 : Fe, Cr, Ni as in case 2. Na as in reference.

TABLE 47

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| Response | Method | MESH | | | |
|---------------------------------|----------|-----------|-----------|----------|----------|
| | | 20 | 62 | 124 | 187 |
| $\phi > 0.1 \text{ MeV}$ DPA | ANISN | 4.03 + 11 | 1.92 + 7 | 2.28 + 1 | 2.15 - 5 |
| | DUCKPOND | 3.89 + 11 | 2.07 + 7 | - | - |
| DPA | ANISN | 1.37 + 14 | 1.29 + 10 | 1.67 + 7 | 2.74 + 4 |
| | DUCKPOND | 1.35 + 14 | 1.57 + 10 | - | - |
| $^{23}\text{Na}(n,\gamma)$ | ANISN | 5.47 + 10 | 2.76 + 7 | 8.07 + 5 | 1.33 + 3 |
| | DUCKPOND | - | - | 2.59 + 6 | 3.87 + 3 |
| $^{59}\text{Co}(n,\gamma)$ | ANISN | 2.43 + 13 | 8.62 + 9 | 7.21 + 7 | 9.55 + 4 |
| | DUCKPOND | - | - | 2.02 + 8 | 2.75 + 5 |
| $^{235}\text{U}(n,f)$ | ANISN | 7.21 + 13 | 3.33 + 10 | 8.01 + 8 | 1.27 + 6 |
| | DUCKPOND | - | - | 2.70 + 9 | 4.06 + 6 |

TABLE 48

UK results using a) ANISN and $1/\xi_f$ weighting for iron (1/E for other isotopes) and b) continuous Monte Carlo (DUCKPOND code). The starting data file is the same (UKNDL) for the two calculations.

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| Group | SUPERTOG | | | MC ² - 2 | | |
|-------|-------------------|--------------------------------|--------------------|---------------------|--------------------------------|--------------------|
| | σ_{inel}^j | $\sigma_{el}(j \rightarrow j)$ | $\sigma_{el}(j+1)$ | σ_{inel}^j | $\sigma_{el}(j \rightarrow j)$ | $\sigma_{el}(j+1)$ |
| 1 | 1.506 | 2.008 | 0.076 | 1.511 | 2.004 | 0.079 |
| 2 | 1.165 | 2.178 | 0.128 | 1.142 | 2.174 | 0.157 |
| 3 | 0.784 | 2.148 | 0.103 | 0.755 | 2.147 | 0.104 |
| 4 | 0.264 | 2.509 | 0.097 | 0.193 | 2.525 | 0.125 |
| 5 | | 1.976 | 0.316 | | 1.959 | 0.348 |
| 6 | | 3.188 | 0.517 | | 3.191 | 0.547 |
| 7 | | 3.439 | 0.159 | | 3.366 | 0.174 |
| 8 | | 2.092 | 1.327 | | 2.054 | 1.430 |
| 9 | | 4.064 | 0.018 | | 4.410 | 0.054 |
| 10 | | 5.367 | 0.593 | | 5.341 | 0.584 |
| 11 | | 11.148 | 0.119 | | 11.229 | 0.118 |
| 12 | | 7.387 | 0.133 | | 7.379 | 0.133 |
| 13 | | 9.916 | 0.200 | | 9.897 | 0.200 |
| 14 | | 11.245 | 0.136 | | 11.248 | 0.136 |
| 15 | - | - | - | - | - | - |

TABLE 49

FE INFINITE DILUTION DATA PROCESSED BY SUPERTOG AND MC² - 2

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DEFINITION OF A FAST BREEDER REACTOR BENCHMARK CONFIGURATION
FOR COMPARISON OF SHIELDING CROSS-SECTION DATA

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- INTRODUCTION -

The benchmark characteristics are specified as follows :

- Section I-VII : benchmark specifications (in particular for the forward flux solution, required for all participants) ;
- Section VIII : uncertainty and sensitivity analysis specifications (optional).

I - GEOMETRY AND COMPOSITIONS -

They are directly obtained from the previous Benchmark definition /1/, as well as the space description (see Appendix I).

II - SOURCES -

The source spectrum is the same of reference /1/, but with the hypothesis of an isotropic angular distribution, to allow calculation at different angular quadrature orders.

The source spectrum is given in the 100 group structure. Both are given in Appendix II. The 100 group structure (DLC-2) is consistent with the following widely used libraries :

| | |
|-----------|--------------|
| VITAMIN-E | (174 groups) |
| VITAMIN-C | (171 ") |
| EURLIB | (100 ") |
| BABEL | (113 ") |
| PROPANE | (45 ") |

If a source redistribution in a fine structure should be necessary, we suggest the following :

$$S_i = S_I \frac{\Delta u_i}{\Delta u_I}$$

where I is the 100 groups structure index and i the finer group index.

III - TRANSPORT CALCULATION -

If the ANISN code is used, we suggest the following selected option values :

| | |
|------------------|--|
| IBL = IBR = 0 | (zero boundary conditions) |
| IFLU = 3 | (weighted mode for difference equations) |
| XLAL = 10^{-3} | convergence tests |
| EPS = 10^{-4} | |

The reference calculation should be $S_4 P_1$ with the angular constants of Appendix III.

IV - CROSS SECTIONS -

It is suggested, in order to simplify the inter-laboratory comparison, to use only one cross section set for each Benchmark region. This will not prevent however to use different "isotope" cross sections in each region (e.g. different Na cross sections in the PNL region, in the pure Na region and in the HE region).

V - PARAMETERS TO BE STUDIED -

The following space-dependent distributions should be considered :

- total flux
- thermal equivalent flux :

$$\phi_{\text{theq}}(r) = \int_0^{\infty} \sqrt{\frac{E_0}{E}} \phi(E, r) dE$$

with $E_0 = .025$ eV, E energy corresponding to the mean group lethargy.

- integral of the flux for energies > 100 KeV :

$$\phi(r)_{>100\text{KeV}} = \int_E 100 > \text{KeV} \phi(E, r) dE$$

- (n, γ) capture rate of ^{23}Na
- (n, γ) capture rate of ^{59}Co
- damage in steel
- (n, f) fission rate of ^{235}U
- γ and neutron heating on the lateral shield
(w/cm^3 of homogeneized composition)

For all these parameters, selected point values should be provided according to the format of Appendix IV.

The calculation of the ^{23}Na and ^{59}Co capture rates and the ^{235}U fission rate, should be performed both with in-house response cross-section and with response cross-section derived from the generally available ENDF/B.V files. In the case of the atomic displacement, beside in-house cross-sections, a standard displacement model (e.g. the NRT model) could be used.

VI - METHOD TESTS -

A few simple method tests are also suggested in order to verify the influence of different cross section data on method approximations :

- a recalculation of the reference with both a doubled space mesh-grid and S_{16} (constants in Appendix III)
- a recalculation of the reference with P_3 option.

VII - TESTING OF DIFFERENT CROSS-SECTION SETS -

To simplify the result interpretation, it is asked that every laboratory participating to the exercice should provide (according to the format described in Appendix V) the following data :

Microscopic cross sections by region :

- 1) Lateral shield : Na, Fe, Cr, Ni
- 2) Pure sodium : Na

in a 15 group structure (see Appendix VI).

This energy structure is the closest possible to the energy structure of the correlation matrices provided by ORNL.

The group collapsing should be performed starting from the reference calculation and using flux weighting algorithms (of the type used in ANISN).

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VIII - SENSITIVITY AND UNCERTAINTY ANALYSIS -

As an option, beside the forward calculation described in Section I-VI, the participants are asked to perform sensitivity calculations for the following two responses :

- Atomic-displacement in Iron at mesh 20 ;
- Sodium activation-rate at mesh 187.

The plotted sensitivity profiles (per unit lethargy) are asked for the elastic and non-elastic cross-sections of Sodium, Iron, Chromium and Nickel.

The sensitivity can be calculated either in the 100-group structure or in the 15-group structure described in Section VII.

Sensitivity profiles could also be calculated for the other responses given in Appendix IV.

For what concerns the uncertainty analysis, the ORNL data (ORNL-5318 Report by JD.Drischler and CR. Weisbin) for Sodium and Iron could be used both directly in the 15 energy group structure, or expanded according to the procedure suggested in the paper "Preliminary version of the EURLIB variance-covariance matrices", by M. Hall (presented at the recent PARIS NEA Meeting), if the sensitivity analysis was performed in the original 100-group structure.

Fractional standard deviations should be provided for the two responses previously mentioned.

REFERENCE /1/ : JY. BARRE : "Benchmark specifications"
see 1976 Vienna Specialist Meeting Proceedings.

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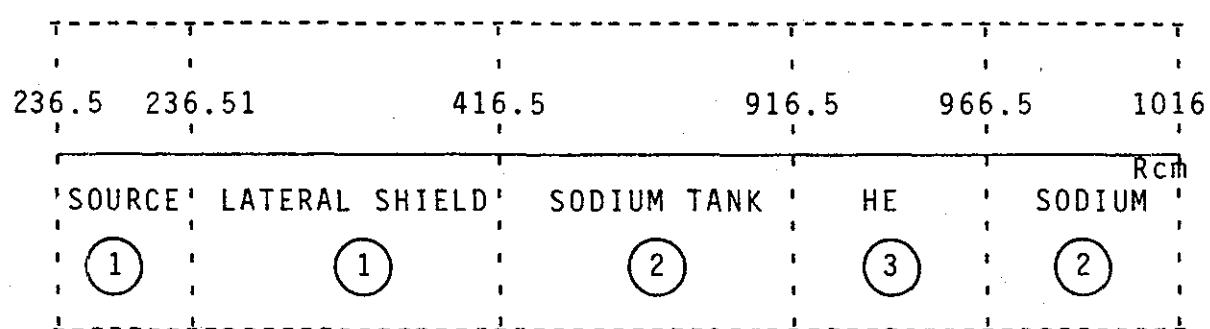
- APPENDIX I -

SPHERICAL GEOMETRY AND COMPOSITIONS

TABLE 1

| ZONE | N° | Inner radius CM | Outer radius CM | Thickness CM | Composition |
|----------------|----|-----------------------|-----------------------|-----------------|-------------|
| Source | 1 | 236.5 | 236.51 | 0.01 | (1) |
| Lateral shield | 2 | 236.51 | 416.5 | 179.99 | (1) |
| Sodium tank | 3 | 416.5 | 916.5 | 500 | (2) |
| HE | 4 | 916.5 | 966.5 | 50 | (3) |
| Sodium | 5 | 966.5 | 1016.5 | 50 | (2) |

FIGURE 1



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TABLE 2

ATOMIC COMPOSITION 10^{24} ATOMS/ CM^3

| REGION | Source and Lateral shield | Sodium tanks | HE |
|---------------------------------------|------------------------------|--------------|--------|
| Composition label | (1) | (2) | (3) |
| % v/o SS* | 53% | 0% | 15% |
| % v/o sodium | 47% | 100% | 85% |
| Atoms/ cm^3 $\times 10^{24}$ | | | |
| Sodium | .01045 | .02223 | .01890 |
| Iron | .03200 | .0 | .00906 |
| Nickel | .00423 | .0 | .00120 |
| Chrome | .00860 | .0 | .00243 |

* Standard SS : \approx 70 - 18 - 12 v/o Fe-Cr-Ni

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TABLE 3
REFERENCE SPACE MESH GRID

| ZONE | Zone number | Total mesh number | Mesh number | Number of meshes | Thickness CM | Radius CM |
|----------------|-------------|-------------------|---------------|------------------|--------------|-----------------|
| Source | 1 | 1 | 1 | 1 | 0.01 | 236.5 236.51 |
| Lateral shield | 2 | 60 | 2 to 61 | 1 59 | 2.99 3.00 | 239.5 416.5 |
| Sodium tank | 3 | 125 | 62 to 186 | 125 | 4.00 | 916.5 |
| HE | 4 | 17 | 187 to 203 | 1 16 | 2.00 3.00 | 918.5 966.5 |
| Sodium | 5 | 13 | 204 to 216 | 1 12 | 2.00 4.00 | 968.5 1016 |

- APPENDIX III -

GROUP STRUCTURE AND SOURCE SPECTRUM

| <u>Group</u> | <u>Energy</u> | <u>Lethargy</u> |
|--------------|---------------|-----------------|
| 1 | 1.3499E 07 | -0.400 à -0.300 |
| 2 | 1.2214E 07 | -0.300 à -0.200 |
| 3 | 1.1052E 07 | -0.200 à -0.100 |
| 4 | 1.0000E 07 | -0.100 à 0.000 |
| 5 | 9.0484E 06 | 0.000 à 0.100 |
| 6 | 8.1873E 06 | 0.100 à 0.200 |
| 7 | 7.4082E 06 | 0.200 à 0.300 |
| 8 | 6.7032E 06 | 0.300 à 0.400 |
| 9 | 6.0653E 06 | 0.400 à 0.500 |
| 10 | 5.4881E 06 | 0.500 à 0.600 |
| 11 | 4.9659E 06 | 0.600 à 0.700 |
| 12 | 4.4933E 06 | 0.700 à 0.800 |
| 13 | 4.0657E 06 | 0.800 à 0.900 |
| 14 | 3.6788E 06 | 0.900 à 1.000 |
| 15 | 3.3287E 06 | 1.000 à 1.100 |
| 16 | 3.0119E 06 | 1.100 à 1.200 |
| 17 | 2.7253E 06 | 1.200 à 1.300 |
| 18 | 2.4660E 06 | 1.300 à 1.400 |
| 19 | 2.2313E 06 | 1.400 à 1.500 |
| 20 | 2.0190E 06 | 1.500 à 1.600 |
| 21 | 1.8268E 06 | 1.600 à 1.700 |
| 22 | 1.6530E 06 | 1.700 à 1.800 |
| 23 | 1.4957E 06 | 1.800 à 1.900 |
| 24 | 1.3534E 06 | 1.900 à 2.000 |
| 25 | 1.2246E 06 | 2.000 à 2.100 |
| 26 | 1.1080E 06 | 2.100 à 2.200 |
| 27 | 1.0026E 06 | 2.200 à 2.300 |
| 28 | 9.0718E 05 | 2.300 à 2.400 |
| 29 | 8.2085E 05 | 2.400 à 2.500 |
| 30 | 7.4274E 05 | 2.500 à 2.600 |
| 31 | 6.7206E 05 | 2.600 à 2.700 |
| 32 | 6.0810E 05 | 2.700 à 2.800 |
| 33 | 5.5023E 05 | 2.800 à 2.900 |
| 34 | 4.9787E 05 | 2.900 à 3.000 |
| 35 | 4.5049E 05 | 3.000 à 3.100 |
| 36 | 4.0762E 05 | 3.100 à 3.200 |
| 37 | 3.6883E 05 | 3.200 à 3.300 |
| 38 | 3.3373E 05 | 3.300 à 3.400 |
| 39 | 3.0197E 05 | 3.400 à 3.500 |
| 40 | 2.7324E 05 | 3.500 à 3.600 |
| 41 | 2.4724E 05 | 3.600 à 3.700 |
| 42 | 2.2371E 05 | 3.700 à 3.800 |
| 43 | 2.0242E 05 | 3.800 à 3.900 |
| 44 | 1.8316E 05 | 3.900 à 4.000 |

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| <u>Group</u> | <u>Energy</u> | <u>Lethargy</u> | |
|--------------|---------------|-----------------|---------------|
| 45 | 1.6573E 05 | 1.8310E 05 | 4.000 4.100 |
| 46 | 1.4996E 05 | 1.6573E 05 | 4.100 4.200 |
| 47 | 1.3569E 05 | 1.4996E 05 | 4.200 4.300 |
| 48 | 1.2277E 05 | 1.3569E 05 | 4.300 4.400 |
| 49 | 1.1109E 05 | 1.2277E 05 | 4.400 4.500 |
| 50 | 8.6517E 04 | 1.1109E 05 | 4.500 4.750 |
| 51 | 6.7379E 04 | 8.6617E 04 | 4.750 5.000 |
| 52 | 5.2475E 04 | 6.7379E 04 | 5.000 5.250 |
| 53 | 4.0868E 04 | 5.2475E 04 | 5.250 5.500 |
| 54 | 3.1828E 04 | 4.0868E 04 | 5.500 5.750 |
| 55 | 2.4788E 04 | 3.1828E 04 | 5.750 6.000 |
| 56 | 1.9305E 04 | 2.4788E 04 | 6.000 6.250 |
| 57 | 1.5034E 04 | 1.9305E 04 | 6.250 6.500 |
| 58 | 1.1709E 04 | 1.5034E 04 | 6.500 6.750 |
| 59 | 9.1188E 03 | 1.1709E 04 | 6.750 7.000 |
| 60 | 7.1017E 03 | 9.1188E 03 | 7.000 7.250 |
| 61 | 5.5308E 03 | 7.1017E 03 | 7.250 7.500 |
| 62 | 4.3074E 03 | 5.5308E 03 | 7.500 7.750 |
| 63 | 3.3546E 03 | 4.3074E 03 | 7.750 8.000 |
| 64 | 2.6126E 03 | 3.3546E 03 | 8.000 8.250 |
| 65 | 2.0347E 03 | 2.6126E 03 | 8.250 8.500 |
| 66 | 1.5846E 03 | 2.0347E 03 | 8.500 8.750 |
| 67 | 1.2341E 03 | 1.5846E 03 | 8.750 9.000 |
| 68 | 9.6112E 03 | 1.2341E 03 | 9.000 9.250 |
| 69 | 7.4852E 02 | 9.6112E 02 | 9.250 9.500 |
| 70 | 5.8295E 02 | 7.4852E 02 | 9.500 9.750 |
| 71 | 4.5400E 02 | 5.8295E 02 | 9.750 10.000 |
| 72 | 3.5357E 02 | 4.5400E 02 | 10.000 10.250 |
| 73 | 2.7536E 02 | 3.5357E 02 | 10.250 10.500 |
| 74 | 2.1445E 02 | 2.7536E 02 | 10.500 10.750 |
| 75 | 1.6702E 02 | 2.1445E 02 | 10.750 11.000 |
| 76 | 1.3007E 02 | 1.6702E 02 | 11.000 11.250 |
| 77 | 1.0130E 02 | 1.3007E 02 | 11.250 11.500 |
| 78 | 7.8893E 01 | 1.0130E 02 | 11.500 11.750 |
| 79 | 6.1442E 01 | 7.8893E 01 | 11.750 12.000 |
| 80 | 4.7851E 01 | 6.1442E 01 | 12.000 12.250 |
| 81 | 3.7267E 01 | 4.7851E 01 | 12.250 12.500 |
| 82 | 2.9023E 01 | 3.7267E 01 | 12.500 12.750 |
| 83 | 2.2603E 01 | 2.9023E 01 | 12.750 13.000 |
| 84 | 1.7603E 01 | 2.2603E 01 | 13.000 13.250 |
| 85 | 1.3710E 01 | 1.7603E 01 | 13.250 13.500 |
| 86 | 1.0677E 01 | 1.3710E 01 | 13.500 13.750 |
| 87 | 8.3153E 00 | 1.0677E 01 | 13.750 14.000 |
| 88 | 6.4760E 00 | 8.3153E 00 | 14.000 14.250 |

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| <u>Group</u> | <u>Energy</u> | <u>Lethargy</u> | |
|--------------|---------------|------------------|---------------|
| 89 | 5.0435E 00 | 6.4760E 00 | 14.250 14.500 |
| 90 | 3.9279E 00 | 5.0435E 00 | 14.500 14.750 |
| 91 | 3.0590E 00 | 3.9279E 00 | 14.750 15.000 |
| 92 | 2.3824E 00 | 3.0590E 00 | 15.000 15.250 |
| 93 | 1.8554E 00 | 2.3824E 00 | 15.250 15.500 |
| 94 | 1.4450E 00 | 1.8554E 00 | 15.500 15.750 |
| 95 | 1.1254E 00 | 1.4450E 00 | 15.750 16.000 |
| 96 | 8.7642E-01 | 1.1254E 00 | 16.000 16.250 |
| 97 | 6.8256E-01 | 8.7642E-01 | 16.250 16.500 |
| 98 | 5.3152E-01 | 6.8256E-01 | 16.500 16.750 |
| 99 | 4.1391E-01 | 5.3152E-01 | 16.750 17.000 |
| 100 | E < 4.1399 ev | 10 ⁻¹ | u > 17.00 |

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ISOTROPIC SOURCE SPECTRUM
COMPONENTS 4 AND 5 OF ANGULAR GRID

| Group N° | $\emptyset 4 = \phi_5$ | Group N° | $\emptyset 4 = \phi_5$ |
|----------|------------------------|----------|------------------------|
| 1 | 6.02524E07 | 51 | 3.27689E12 |
| 2 | 1.81727E08 | 52 | 2.34726E12 |
| 3 | 4.07211E08 | 53 | 3.46194E12 |
| 4 | 9.42370E08 | 54 | 3.26389E12 |
| 5 | 1.95173E09 | 55 | 3.84814E12 |
| 6 | 3.52236E09 | 56 | 3.92430E12 |
| 7 | 6.27127E09 | 57 | 2.52851E12 |
| 8 | 9.84427E09 | 58 | 2.76140E12 |
| 9 | 1.58784E10 | 59 | 2.69055E12 |
| 10 | 2.08818E10 | 60 | 1.87633E12 |
| 11 | 3.05881E10 | 61 | 1.86242E12 |
| 12 | 3.57854E10 | 62 | 1.60780E12 |
| 13 | 4.37794E10 | 63 | 9.22607E11 |
| 14 | 4.27307E10 | 64 | 2.26337E11 |
| 15 | 5.09825E10 | 65 | 1.15389E12 |
| 16 | 7.42581E10 | 66 | 1.57888E12 |
| 17 | 9.74418E10 | 67 | 1.43406E12 |
| 18 | 1.08859E11 | 68 | 1.17007E12 |
| 19 | 1.31778E11 | 69 | 9.04616E11 |
| 20 | 1.12294E11 | 70 | 7.21524E11 |
| 21 | 1.06088E11 | 71 | 5.61813E11 |
| 22 | 1.19919E11 | 72 | 3.85968E11 |
| 23 | 1.22713E11 | 73 | 2.63066E11 |
| 24 | 1.43676E11 | 74 | 2.07377E11 |
| 25 | 1.38604E11 | 75 | 1.50525E11 |
| 26 | 1.68639E11 | 76 | 1.43630E11 |
| 27 | 1.21492E11 | 77 | 3.99921E10 |
| 28 | 1.37396E11 | 78 | 8.70758E10 |
| 29 | 2.31932E11 | 79 | 2.03617E10 |
| 30 | 3.17939E11 | 80 | 5.84330E10 |
| 31 | 3.58870E11 | 81 | 6.25251E10 |
| 32 | 4.61146E11 | 82 | 8.45539E09 |
| 33 | 5.45901E11 | 83 | 3.26659E10 |
| 34 | 6.05226E11 | 84 | 1.89189E09 |
| 35 | 4.10883E11 | 85 | 2.17767E10 |
| 36 | 3.35203E11 | 86 | 3.09199E10 |
| 37 | 4.14334E11 | 87 | 3.41943E10 |
| 38 | 6.16085E11 | 88 | 5.53856E08 |
| 39 | 6.74255E11 | 89 | 4.99411E09 |
| 40 | 7.75847E11 | 90 | 1.45122E10 |
| 41 | 7.73701E11 | 91 | 1.68612E10 |
| 42 | 8.05348E11 | 92 | 1.70436E10 |
| 43 | 7.97731E11 | 93 | 1.59551E10 |
| 44 | 9.60821E11 | 94 | 1.42725E10 |
| 45 | 8.96930E11 | 95 | 1.20954E10 |
| 46 | 9.01712E11 | 96 | 9.80882E09 |
| 47 | 1.07587E12 | 97 | 7.67665E09 |
| 48 | 1.07842E12 | 98 | 5.62878E09 |
| 49 | 1.09122E12 | 99 | 3.58773E09 |
| 50 | 2.90643E12 | 100 | 2.17189E09 |

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- APPENDIX III -

ANGULAR DATA FOR S_N CALCULATIONS

S₄ Calculations :

| ANGULAR QUADRATURE CONSTANTS | | |
|------------------------------|-------------|----------------|
| COSINE (MU) | WEIGHT | REFL DIRECTION |
| - 1.00000E+00 | 0 | 5 |
| - 8.61130E-01 | 1.73400E-01 | 5 |
| - 3.39980E-01 | 3.26570E-01 | 4 |
| 3.39980E-01 | 3.26570E-01 | 3 |
| 8.61130E-01 | 1.73400E-01 | 2 |

S₁₆ Calculations :

| ANGULAR QUADRATURE CONSTANTS | | |
|------------------------------|-------------|----------------|
| COSINE (MU) | WEIGHT. | REFL DIRECTION |
| - 1.00000E+00 | 0 | 17 |
| - 9.89400E-01 | 1.35760E-02 | 17 |
| - 9.44574E-01 | 3.11270E-02 | 16 |
| - 8.65630E-01 | 4.75790E-02 | 15 |
| - 7.55404E-01 | 6.23140E-02 | 14 |
| - 6.17876E-01 | 7.47979E-02 | 13 |
| - 4.58017E-01 | 8.45779E-02 | 12 |
| - 2.81604E-01 | 9.13010E-02 | 11 |
| - 9.50129E-02 | 9.47250E-02 | 10 |
| 9.50129E-02 | 9.47250E-02 | 9 |
| 2.81604E-01 | 9.13010E-02 | 8 |
| 4.58017E-01 | 8.45779E-02 | 7 |
| 6.17876E-01 | 7.47979E-02 | 6 |
| 7.55404E-01 | 6.23140E-02 | 5 |
| 8.65630E-01 | 4.75790E-02 | 4 |
| 9.44574E-01 | 3.11270E-02 | 3 |
| 9.89400E-01 | 1.35760E-02 | 2 |

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- APPENDIX IV -

| | Lateral shield interval | | Sodium tank interval | |
|---------------------------------|-------------------------|----|----------------------|-----|
| | 20 | 62 | 124 | 187 |
| ϕ_{total} | | | | |
| $\phi_{th\ eq}$ | | | | |
| $\phi > 100\text{ KeV}$ | | | | |
| $^{23}Na(n,\gamma)$ | | | | |
| $^{59}Co(n,\gamma)$ | | | | |
| $^{235}U(n,f)$ | | | | |
| DPA | | | | |
| γ -heating (w/cm^3) | | | | |
| neutron heating (w/cm^3) | | | | |
| Total heating (w/cm^3) | | | | |

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- A P P E N D I X V -

Data format (Data to be sent as punched cards) should be the standard ANISN format, with :

IHM = 20

IHT = 5

IHS = 6

Position 1 and 2 can be used for $\sigma(n,\gamma)$ (Position 2) and for total inelastic, if available (Position 1).

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- APPENDIX VI -

15 ENERGY GROUP STRUCTURE FOR SENSITIVITY CALCULATIONS

| Group | E_{lower} for group |
|-------|-----------------------|
| 1 | 4.49 MeV |
| 2 | 2.59 |
| 3 | 1.35 |
| 4 | .706 |
| 5 | .578 |
| 6 | .407 |
| 7 | .302 |
| 8 | .273 |
| 9 | 67.4 KeV |
| 10 | 31.8 |
| 11 | 15.0 |
| 12 | 1.58 |
| 13 | 214 eV |
| 14 | 10.7 |
| 15 | down to thermal |

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Specialists' Meeting on Shielding Benchmark Calculations1st and 2nd July, 1982, OECD, ParisLIST OF PARTICIPANTS AND CONTRIBUTORSTO THE SHIELDING BENCHMARKS

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